



HBT-EP research supported
by U.S. DOE Grant
DE-FG02-86ER53222



Measurement of scrape-off-layer current dynamics during MHD activity and disruptions in HBT-EP

Jeffrey P. Levesque

with the HBT-EP Group:

J.W. Brooks¹, M.C. Abler¹, J. Bialek¹, S. DeSanto¹, C.J. Hansen²,
P.E. Hughes^{1,3}, M.E. Mael¹, G.A. Navratil¹, and I.G. Stewart¹

¹ Columbia University

² University of Washington

³ Princeton Plasma Physics Lab



July 17, 2017

Key results in HBT-EP*



- Direct measurements of toroidal vessel currents reveal asymmetric, oscillating *co-* and *counter-* I_p wall currents during kink modes and disruptions
 - Insulating breaks constrain vessel current to complete its circuit through SOL plasma
 - Currents reach $\sim 4\%$ of I_p during disruptions.
- I_p asymmetry characteristics agree with JET results¹ and ITER modeling²
 - Slope of asymmetry $\Delta I_p / \Delta M_{IR,IZ}$ scales like $1/a$
- Wall touching kink mode (WTKM)³ and Asymmetric toroidal eddy current (ATEC)⁴ models can qualitatively explain some HBT-EP measurements, but each model is incomplete as formulated.
 - *Both* ATEC and WTKM concepts are significant for vessel currents
 - Both models also have problems explaining some of the observations
 - Each model can qualitatively explain observed plasma current asymmetries
 - Conditions for ATEC appear more restrictive overall

[1] Gerasimov S.N. *et al.*, *Nucl. Fusion* **54** 073009 (2014)
[2] Roccella R. *et al.*, “Modelling ITER asymmetric VDEs through asymmetries of toroidal eddy currents” IAEA FEC [EX/P6-40] (2016)

[3] Zakharov L.E. *et al.*, *Phys. Plasmas* **19** 055703 (2012)
[4] Roccella R. *et al.*, *Nucl. Fusion* **56** 106010 (2016)

* Levesque, J.P. *et al.*, *Nucl. Fusion* **57** 086035 (2017)

Outline



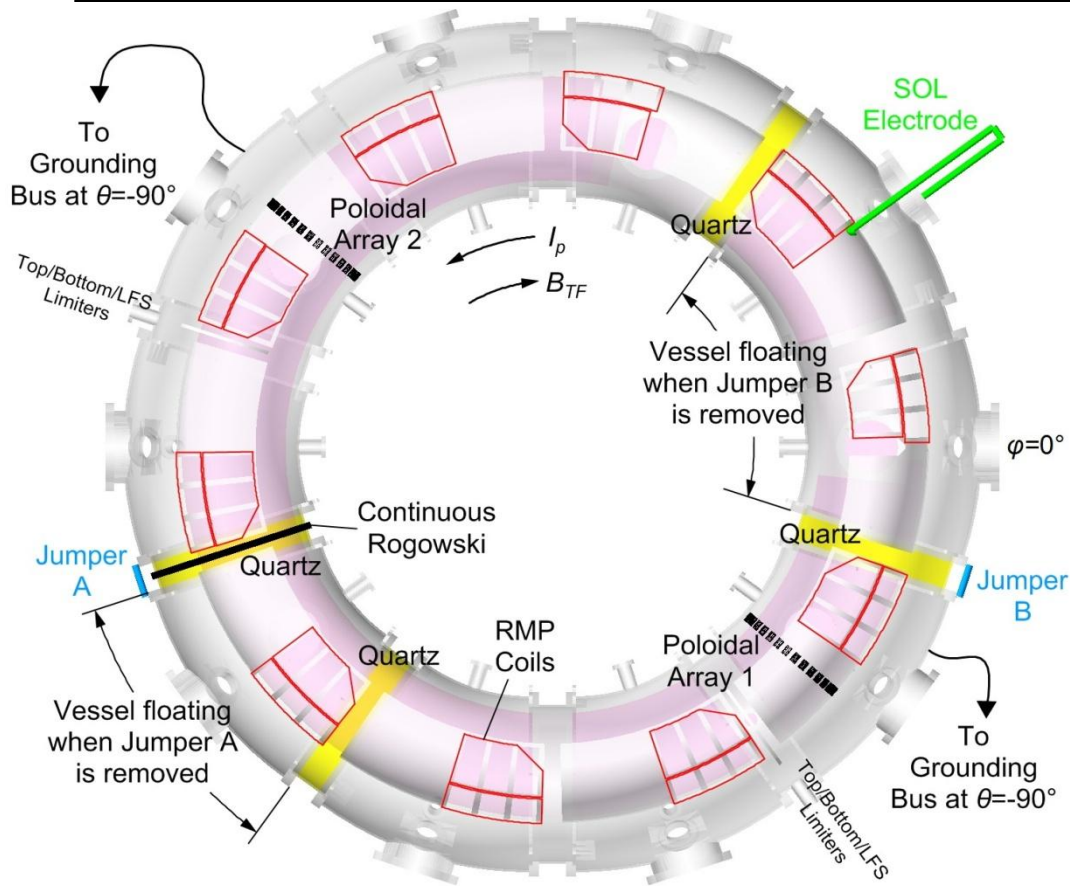
- HBT-EP device overview
 - Scrape-off layer current (SOLC) diagnostics and vessel geometry
 - Discharge characteristics
- Measurements during routine kink mode activity
- Measurements during disruptions
- Interpretation in context of WTKM and ATEC models
- Upcoming simulation and experiments

Outline



- HBT-EP device overview
 - Scrape-off layer current (SOLC) diagnostics and vessel geometry
 - Discharge characteristics
- Measurements during routine kink mode activity
- Measurements during disruptions
- Interpretation in context of WTKM and ATEC models
- Upcoming simulation and experiments

SOL current diagnostics on HBT-EP

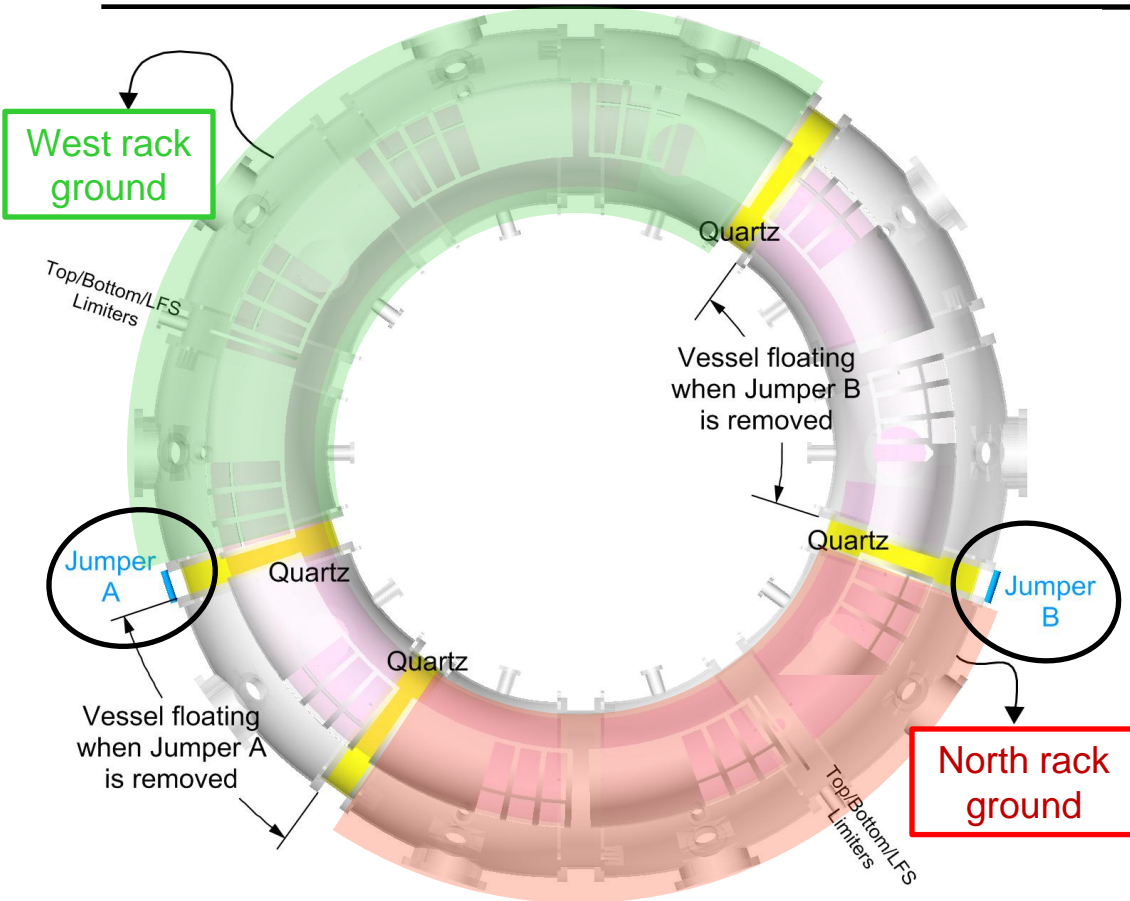


- Isolated chamber sections
- Jumpers between isolated vessel sections
- Poloidal arrays of B_θ sensors
- Grounded electrode in the SOL

Typical discharge parameters

Major Radius:	92 cm
Minor Radius:	15 cm
Plasma Current:	~15 kA
Toroidal Field:	0.33 T
Pulse Length:	5 - 10 ms
Electron Temperature:	≤ 150 eV

SOL current diagnostics on HBT-EP

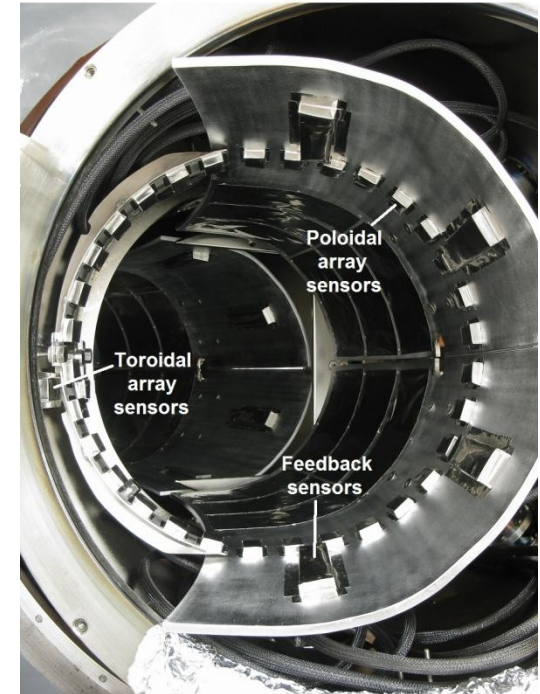
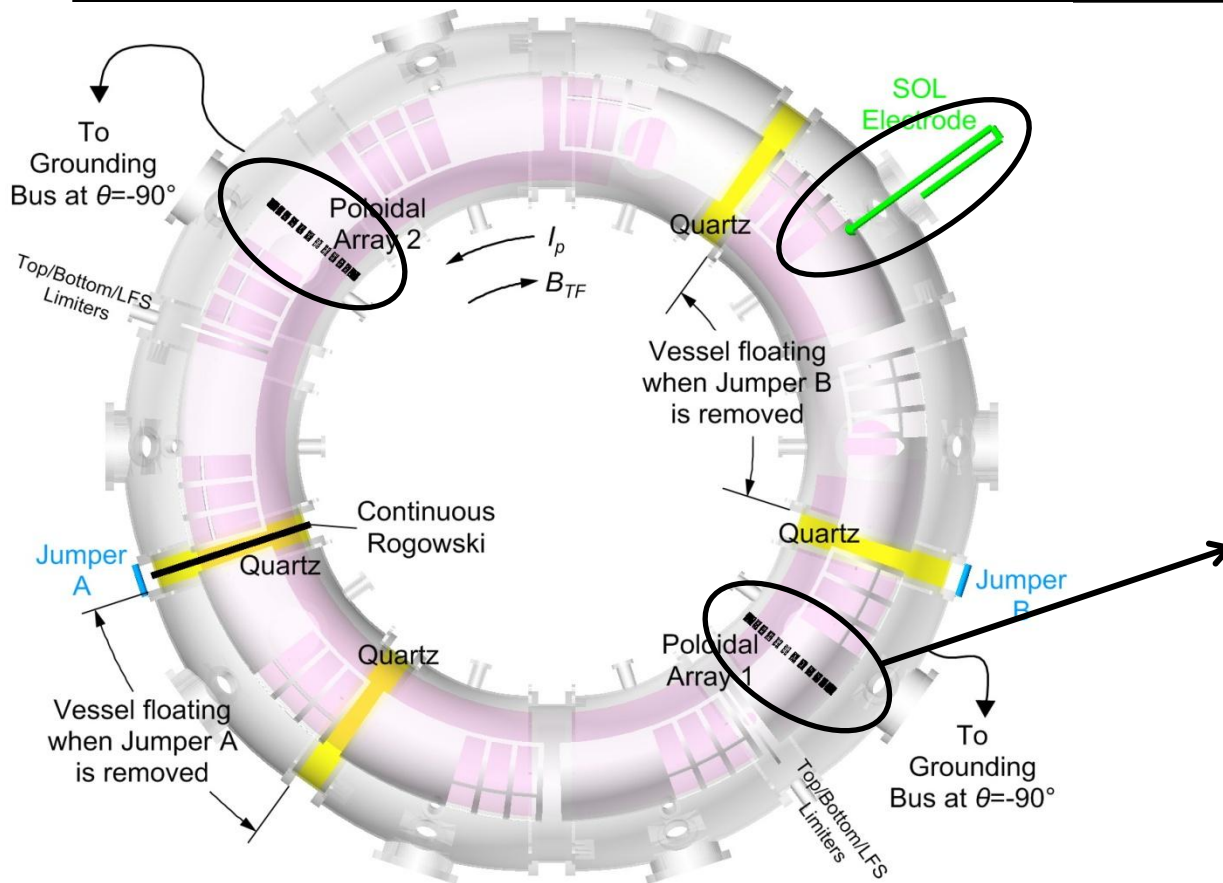


- Isolated chamber sections
- Jumpers between isolated vessel sections
- Poloidal arrays of B_θ sensors
- Grounded electrode in the SOL

Typical discharge parameters

Major Radius:	92 cm
Minor Radius:	15 cm
Plasma Current:	~15 kA
Toroidal Field:	0.33 T
Pulse Length:	5 - 10 ms
Electron Temperature:	≤ 150 eV

SOL current diagnostics on HBT-EP



- Isolated chamber sections
- Jumpers between isolated vessel sections
- Poloidal arrays of B_θ sensors
- Grounded electrode in the SOL

Typical discharge parameters

Major Radius:	92 cm
Minor Radius:	15 cm
Plasma Current:	~15 kA
Toroidal Field:	0.33 T
Pulse Length:	5 - 10 ms
Electron Temperature:	≤ 150 eV

SOL current diagnostics on HBT-EP



- Poloidal arrays measure I_p asymmetry and current moments:

Plasma current at each φ : $I_p^{\text{PA}p} = \oint \vec{B} \cdot d\vec{l} / \mu_0$

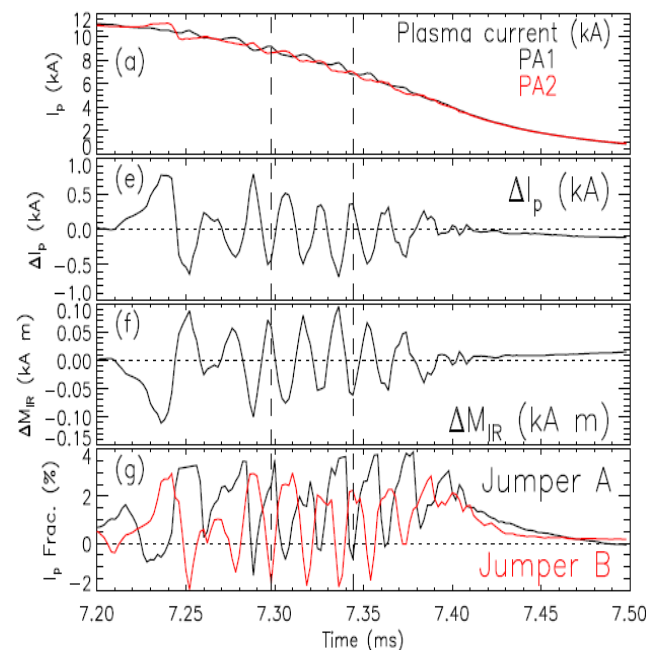
Plasma current asymmetry: $\Delta I_p = I_p^{\text{PA}2p} - I_p^{\text{PA}1p}$

Fractional I_p asymmetry: $f_{\text{PA}}^{\text{asym}} = 2\Delta I_p / (I_p^{\text{PA}2p} + I_p^{\text{PA}1p})$

Vertical current moment: $M_{\text{IZ}} \equiv \int Z j_{\text{plasma}} dR dZ$

Radial current moment: $M_{\text{IR}} \equiv \int (R - R_{\text{cent}}) j_{\text{plasma}} dR dZ$
 $= \sum B_{\theta i} (R_i - R_{\text{cent}}) dl_i / \mu_0$

Radial moment asymmetry: $\Delta M_{\text{IR}} = M_{\text{IR}}^{\text{PA}2p} - M_{\text{IR}}^{\text{PA}1p}$

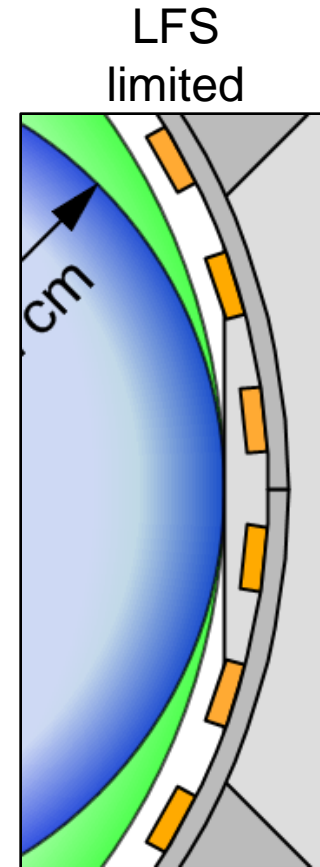
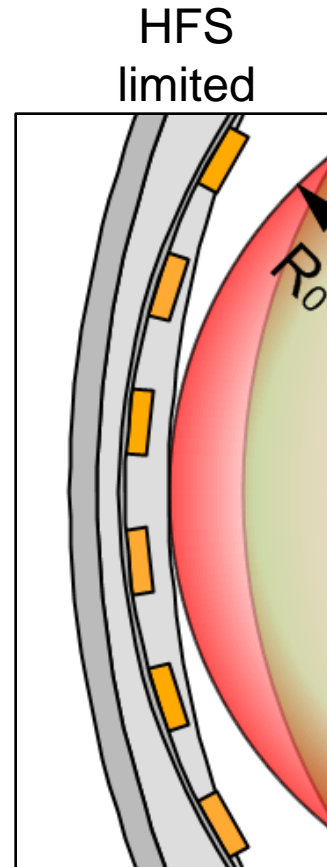
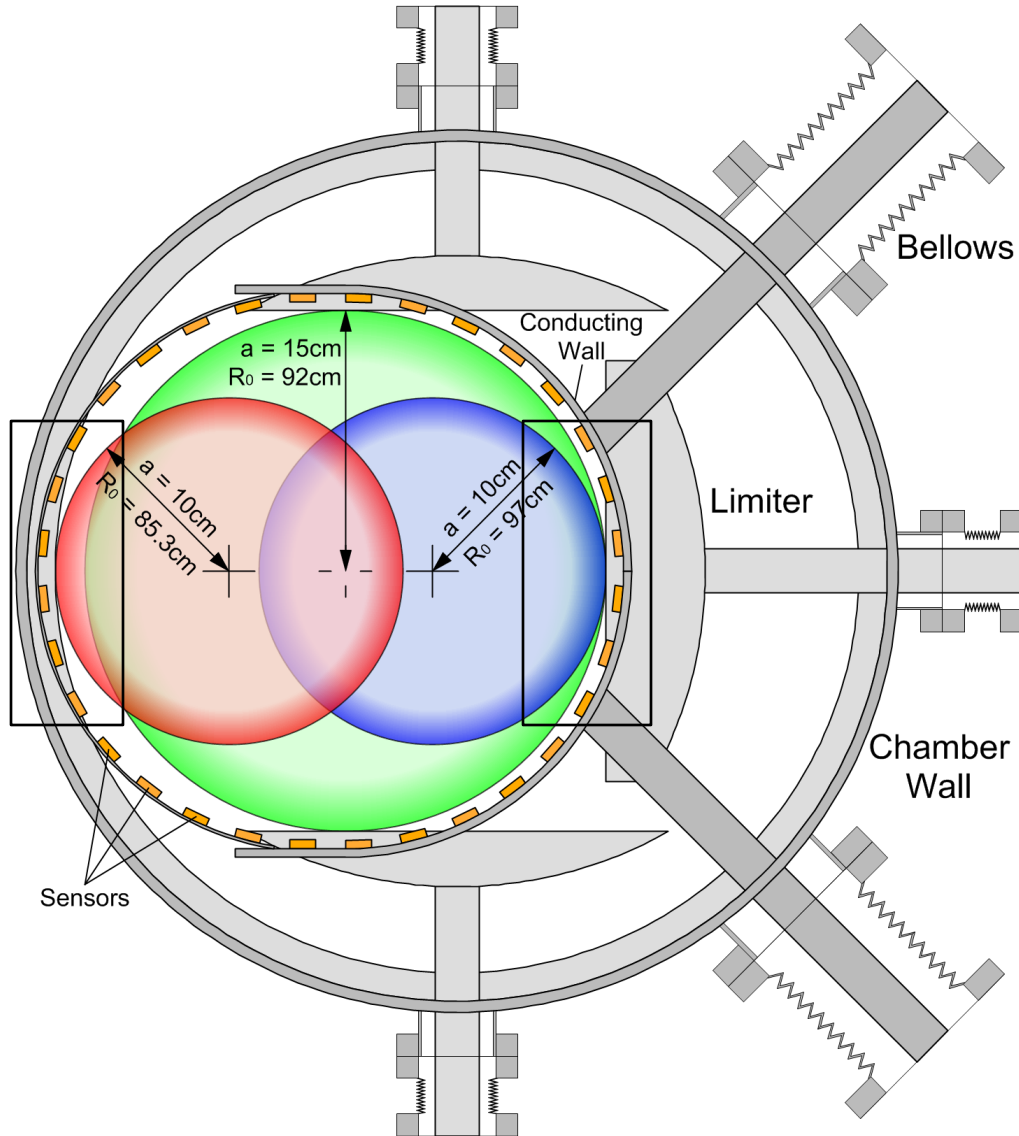


- Jumpers across quartz breaks directly measure toroidal vessel current

- Positive current defined as co- I_p

- Fractional current is normalized to plasma current: $f_{A,B}^{\text{jumper}} = I_{A,B}^{\text{jumper}} / I_p$

HFS- and LFS-limited plasmas have only ~1cm thick vacuum/SOL region between LCFS and magnetic sensors



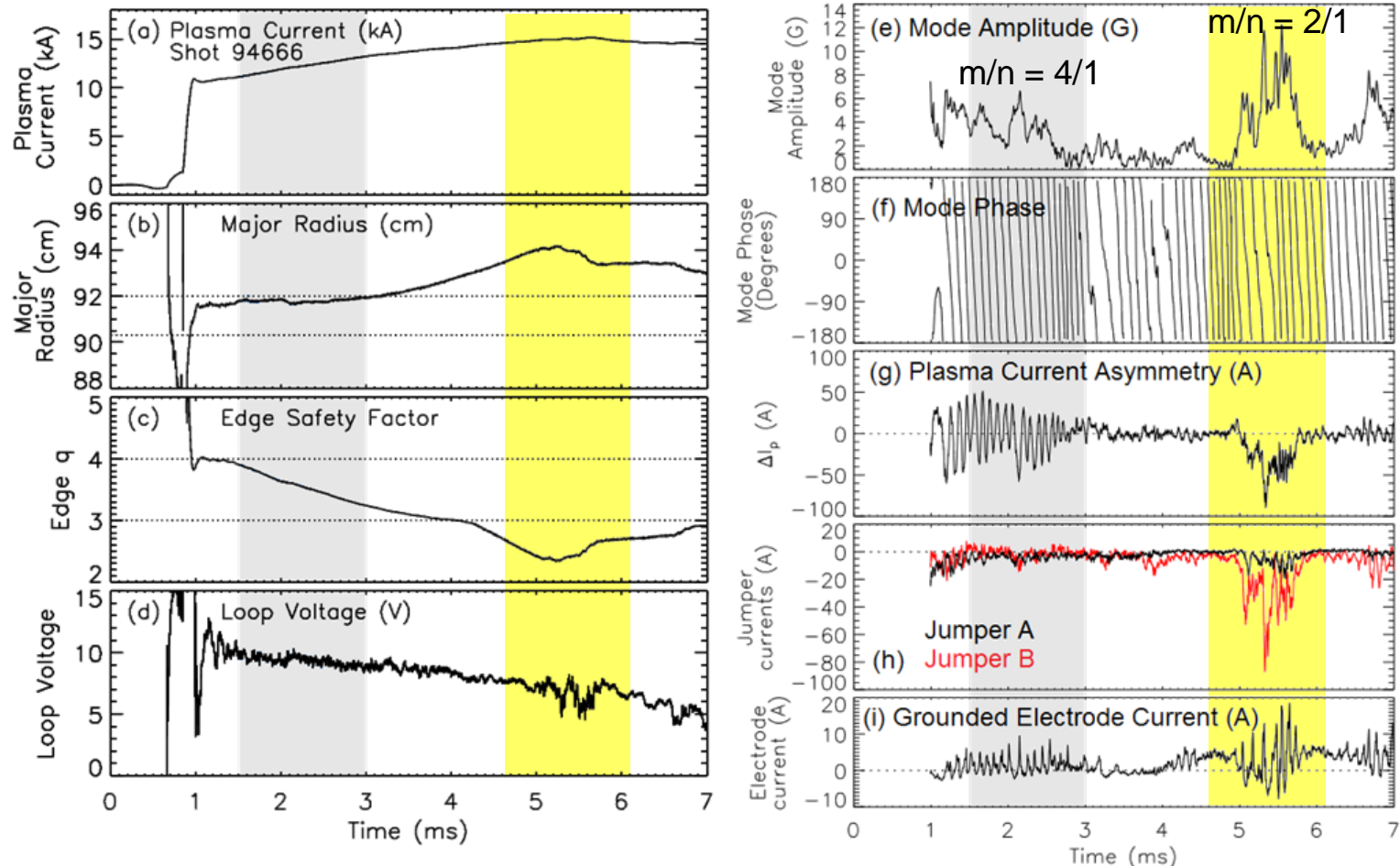
- Limiting surfaces are at different toroidal angles than the sensors

Outline



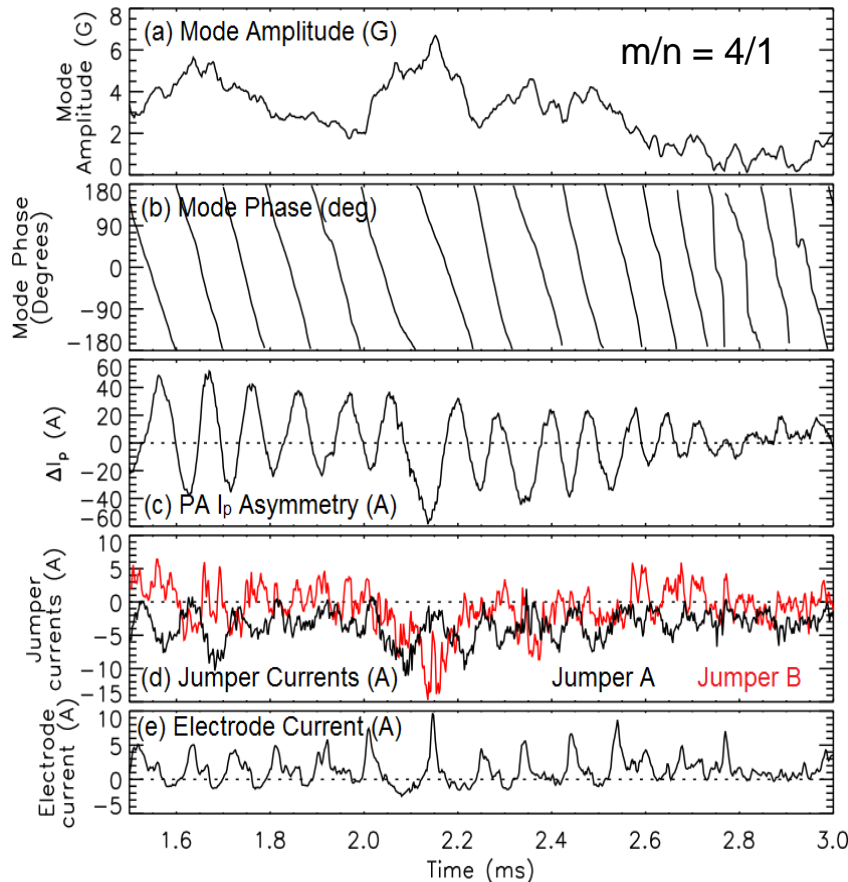
- HBT-EP device overview
 - Scrape-off layer current (SOLC) diagnostics and vessel geometry
 - Discharge characteristics
- **Measurements during routine kink mode activity**
- Measurements during disruptions
- Interpretation in context of WTKM and ATEC models
- Upcoming simulation and experiments

MHD modes during main discharge are accompanied by I_p asymmetries and driven vessel currents that must conduct through the SOL



- An $m/n=4/1$ kink mode initiates after startup, then decays as q_* decreases
- An $m/n=2/1$ mode appears later at lower q_*
- SOL current features are different for each mode and diagnostic

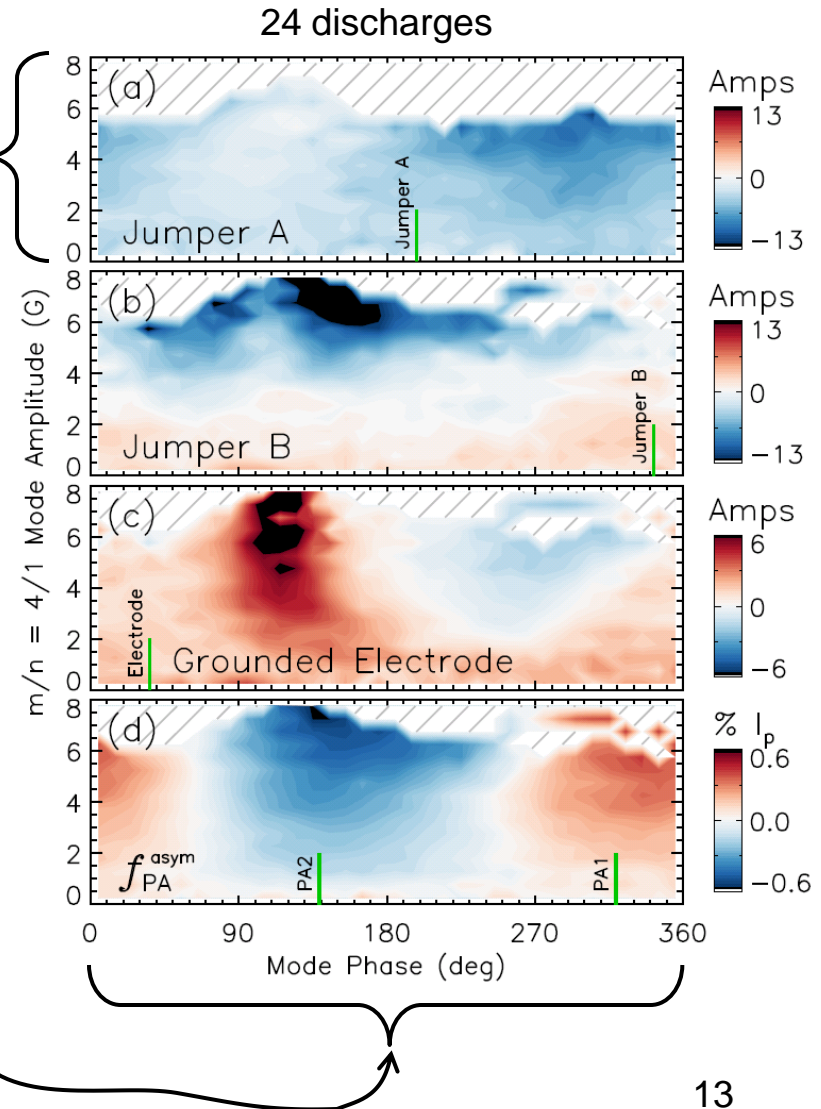
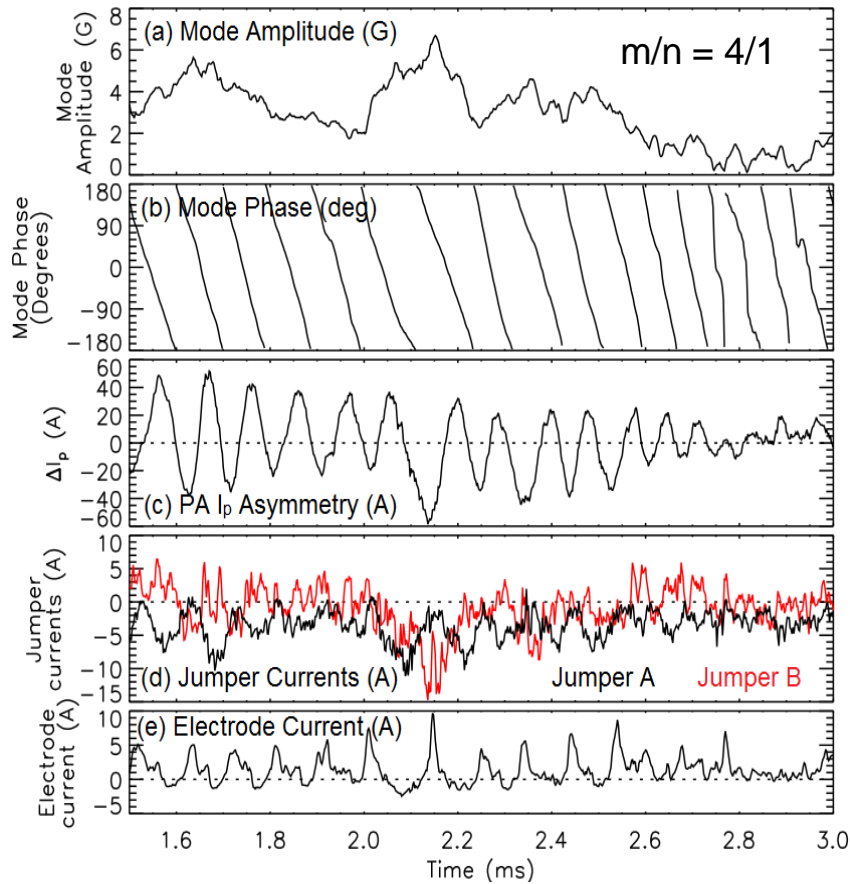
MHD modes during main discharge are accompanied by I_p asymmetries and driven vessel currents that must conduct through the SOL



For the initial 4/1 mode:

- SOL currents are modulated by mode amplitude and phase
 - Stronger currents for larger mode amplitudes
- I_p asymmetry of up to 0.5%
- Toroidal Jumper currents are mostly counter- I_p (negative)
- Grounded electrode measures brief current spikes
 - Positive current for collecting electrons

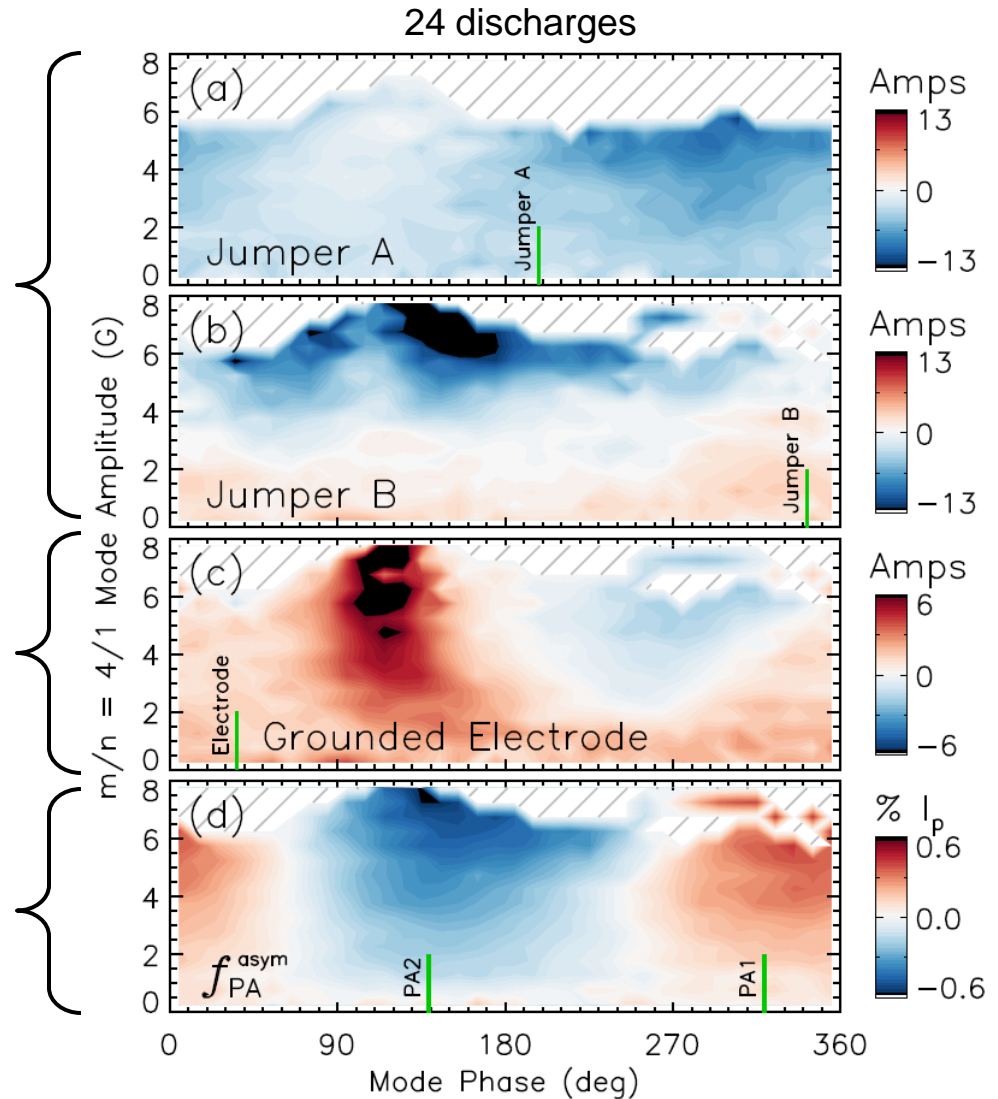
I_p asymmetry and driven vessel current behavior is consistent for early 4/1 modes in each discharge



I_p asymmetry and driven vessel current behavior is consistent for early 4/1 modes in each discharge



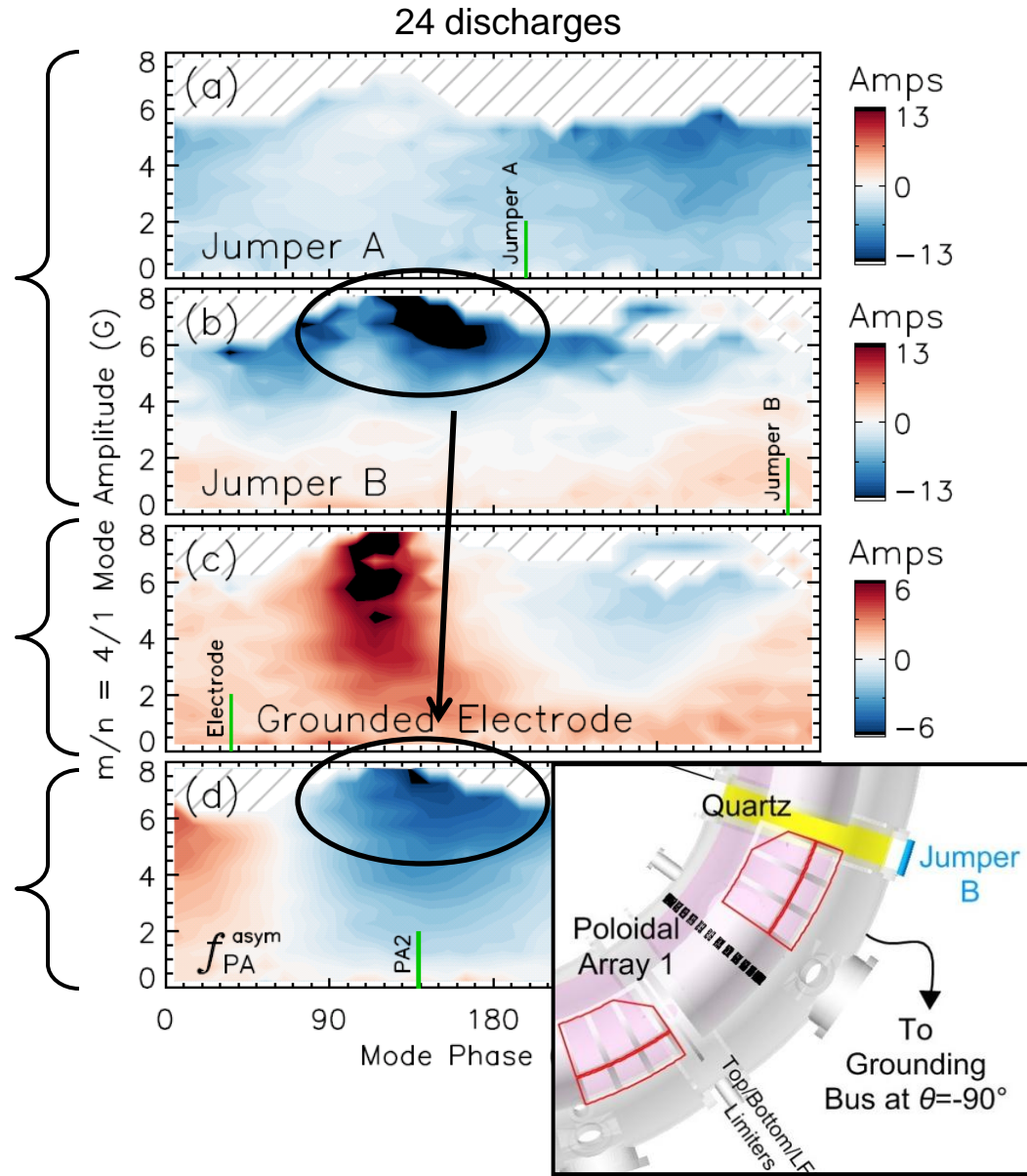
- Toroidal jumper currents are weak ($\sim 0.1\%$ of I_p) and mostly counter- I_p in response to larger modes
- Grounded SOL electrode collects largest electron current when δB_r is maximum at the probe location
- Each poloidal array measures elevated I_p when the nearby jumper current is counter- I_p



I_p asymmetry and driven vessel current behavior is consistent for early 4/1 modes in each discharge



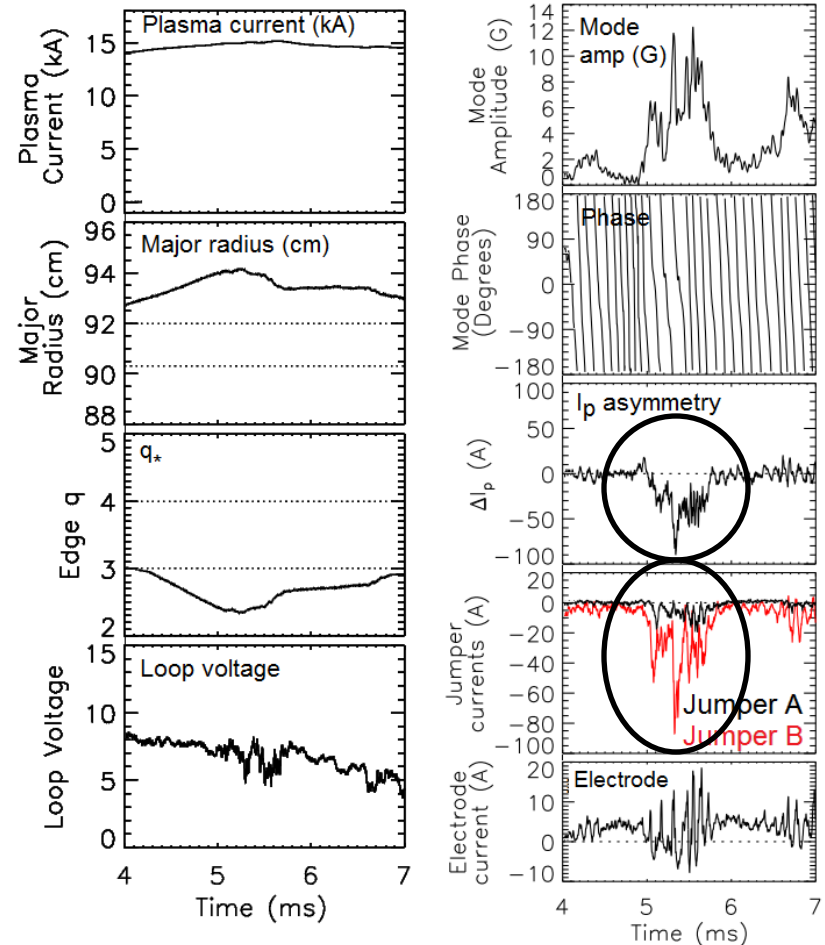
- Toroidal jumper currents are weak ($\sim 0.1\%$ of I_p) and mostly counter- I_p in response to larger modes
- Grounded SOL electrode collects largest electron current when δB_r is maximum at the probe location
- Each poloidal array measures elevated I_p when the nearby jumper current is counter- I_p



Later $m/n=2/1$ modes have different features

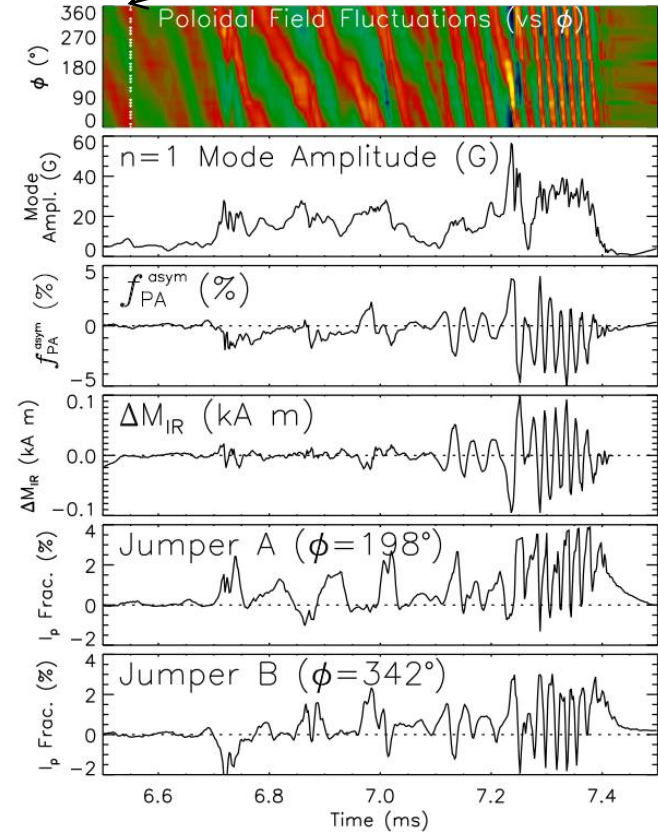
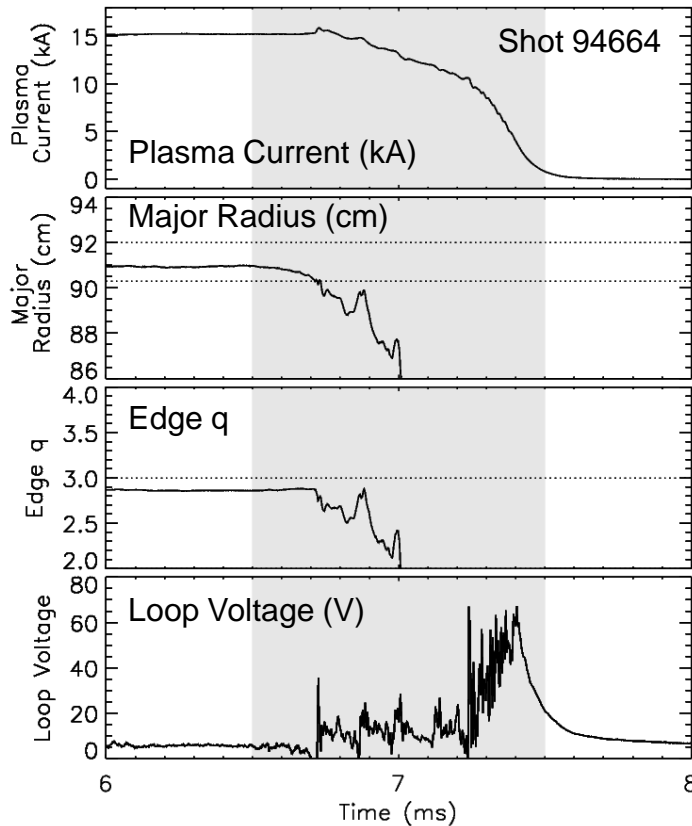
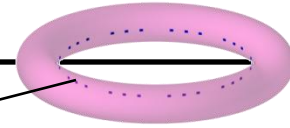


- During rotation of a strong transient $2/1$ mode, I_p asymmetry *does not* rotate
 - I_p remains elevated on one side of tokamak despite several periods of mode rotation
- Jumper B measures much stronger current than Jumper A throughout rotation



-
- HBT-EP device overview
 - Scrape-off layer current (SOLC) diagnostics and vessel geometry
 - Discharge characteristics
 - Measurements during routine kink mode activity
 - **Measurements during disruptions**
 - Interpretation in context of WTKM and ATEC models
 - Upcoming simulation and experiments

Disruptions yield large asymmetries in plasma current and toroidal vessel currents

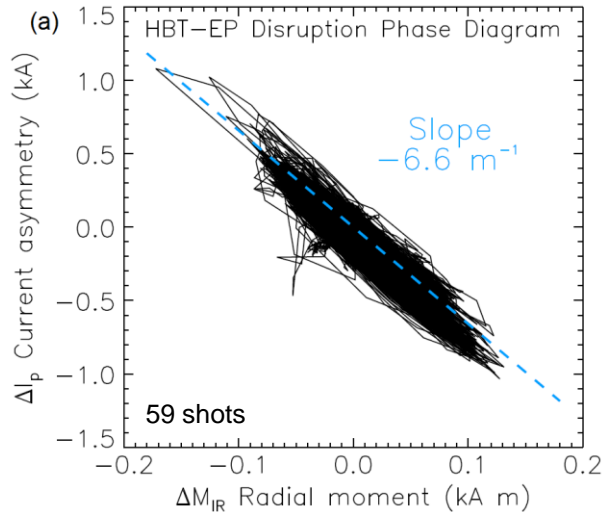


- Asymmetric field $\delta B_{\theta}/B_{\theta}$ reaches 20%
- Jumper currents and I_p asymmetry are $\sim 5\%$ of pre-disruption I_p
- Halo current rotation is much faster than in larger tokamaks
 - Generally above 20kHz, rather than below 2kHz

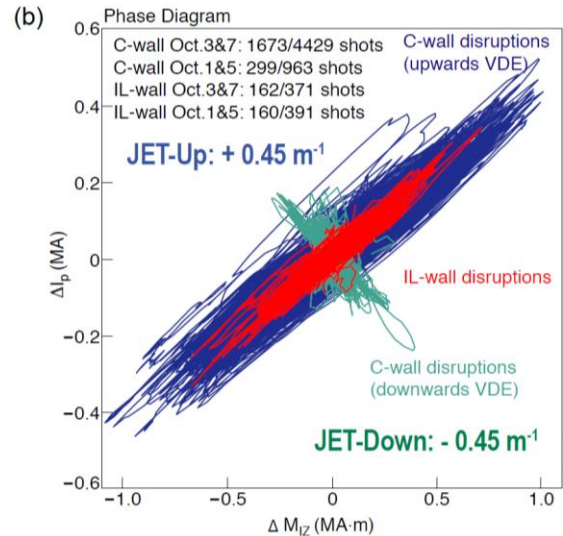
Plasma current asymmetries scale with displacement of current centroid toward the vessel wall



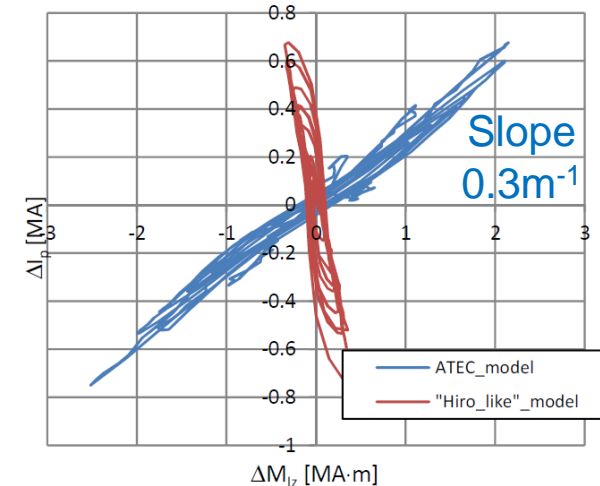
HBT-EP



JET¹



ITER²



- Relation between ΔI_p and ΔM_I asymmetries agree with JET measurements and ITER predictions using ATEC model
 - Opposite pitch is due to which direction gives motion into the wall
- Slope scales as $\sim 1/a$ characteristic for each tokamak

[1] Gerasimov S.N. *et al.*, *Nucl. Fusion* **54** 073009 (2014)

[2] Roccella R. *et al.*, "Modelling ITER asymmetric VDEs through asymmetries of toroidal eddy currents" IAEA FEC [EX/P6-40] (2016)

Different SOL current characteristics at varying stages of disruptions

1. Current spike

- Toroidal jumpers usually measure a counter- I_p spike, but occasionally measure co- I_p spikes.
 - Co- I_p spike occurs when plasma is HFS-limited

2. Slow I_p decay

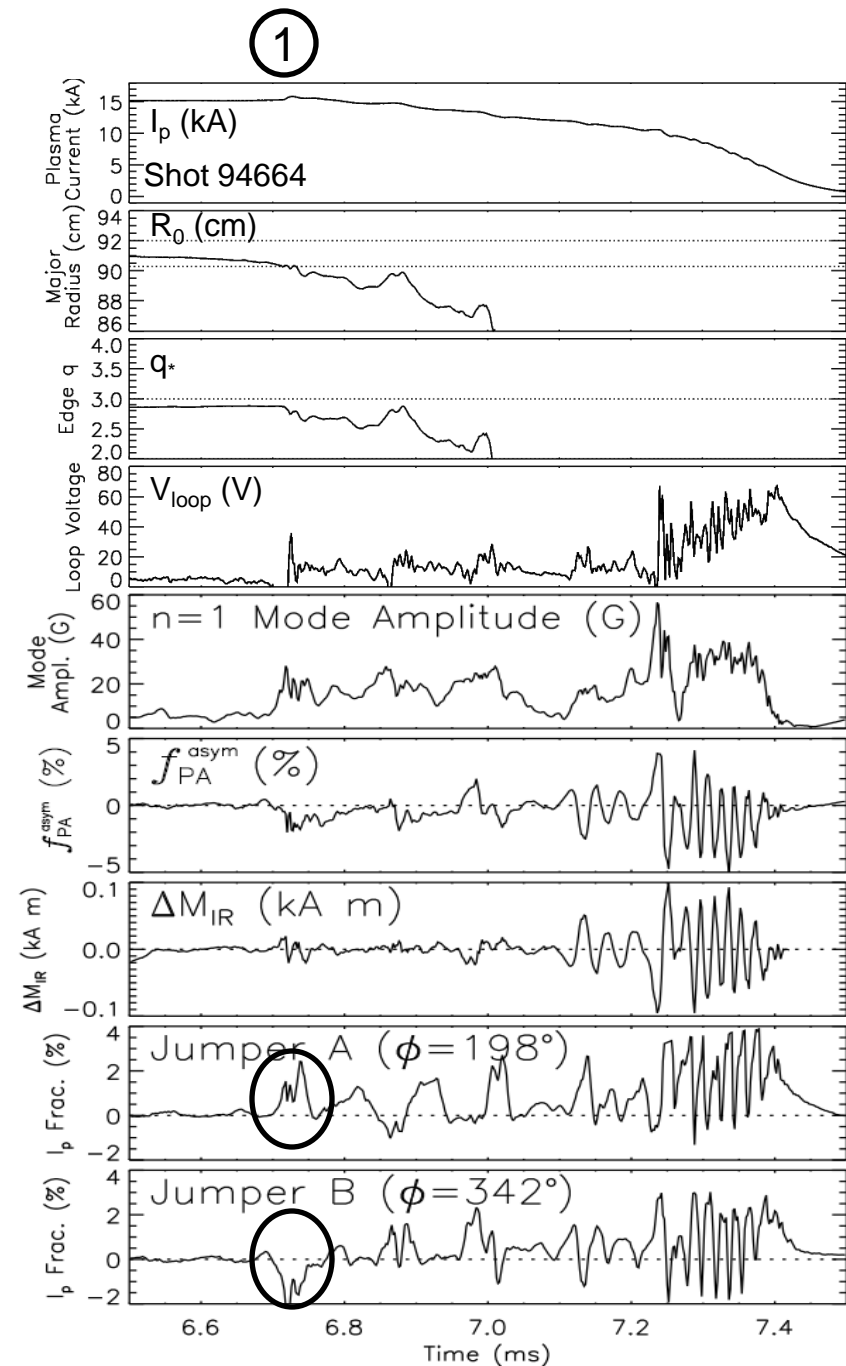
- Mode rotates at 10-20kHz
- Rotation is irregular

3. Fast I_p decay

- Fast halo current rotation at ~50kHz
- Rotation is smooth

4. Symmetric vessel currents

- Co- I_p vessel currents conduct across insulating breaks after mode decays



Different SOL current characteristics at varying stages of disruptions

1. Current spike

- Toroidal jumpers usually measure a counter- I_p spike, but occasionally measure co- I_p spikes.
 - Co- I_p spike occurs when plasma is HFS-limited

2. Slow I_p decay

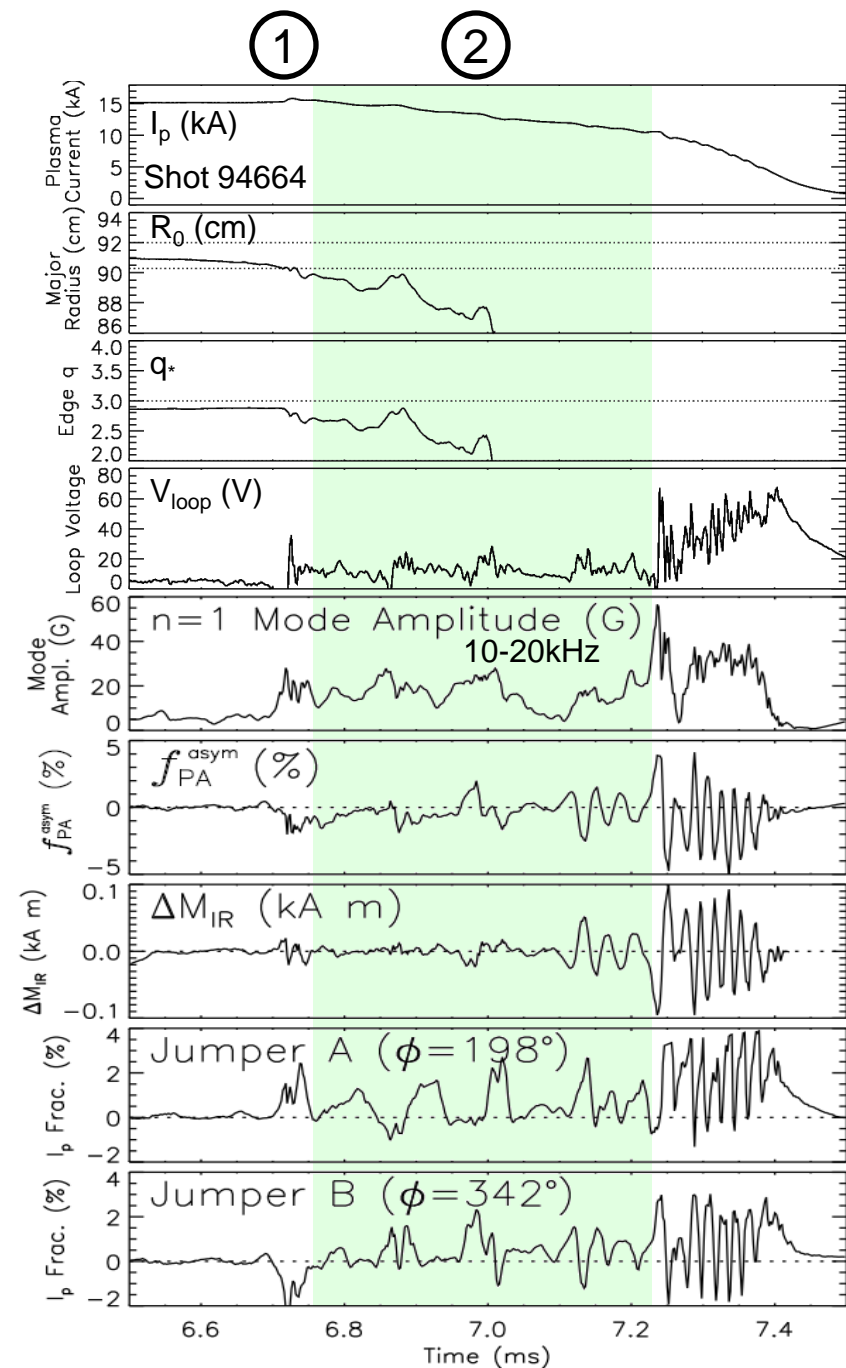
- Mode rotates at 10-20kHz
- Rotation is irregular

3. Fast I_p decay

- Fast halo current rotation at ~50kHz
- Rotation is smooth

4. Symmetric vessel currents

- Co- I_p vessel currents conduct across insulating breaks after mode decays



Different SOL current characteristics at varying stages of disruptions

1. Current spike

- Toroidal jumpers usually measure a counter- I_p spike, but occasionally measure co- I_p spikes.
 - Co- I_p spike occurs when plasma is HFS-limited

2. Slow I_p decay

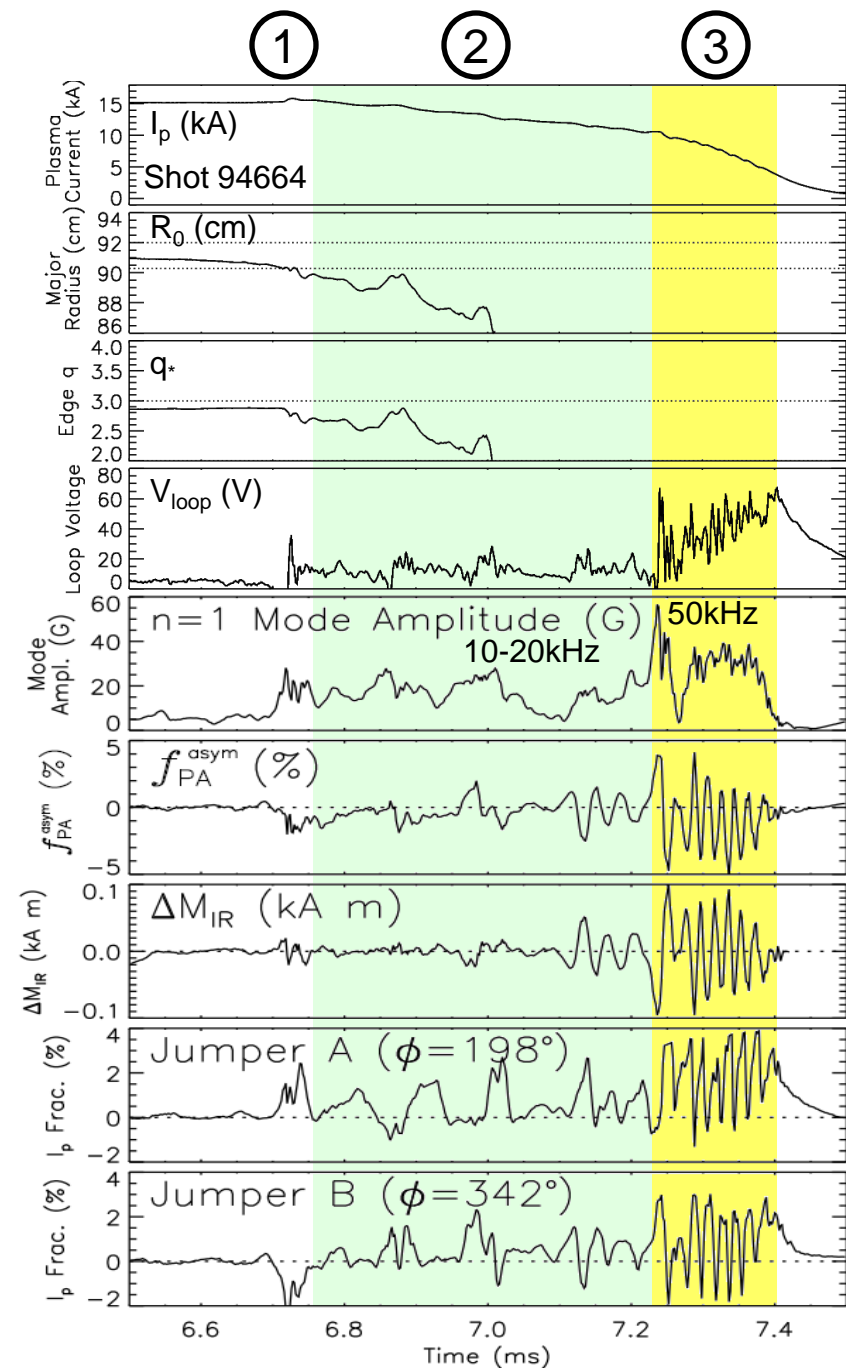
- Mode rotates at 10-20kHz
- Rotation is irregular

3. Fast I_p decay

- Fast halo current rotation at ~50kHz
- Rotation is smooth

4. Symmetric vessel currents

- Co- I_p vessel currents conduct across insulating breaks after mode decays



Different SOL current characteristics at varying stages of disruptions

1. Current spike

- Toroidal jumpers usually measure a counter- I_p spike, but occasionally measure co- I_p spikes.
 - Co- I_p spike occurs when plasma is HFS-limited

2. Slow I_p decay

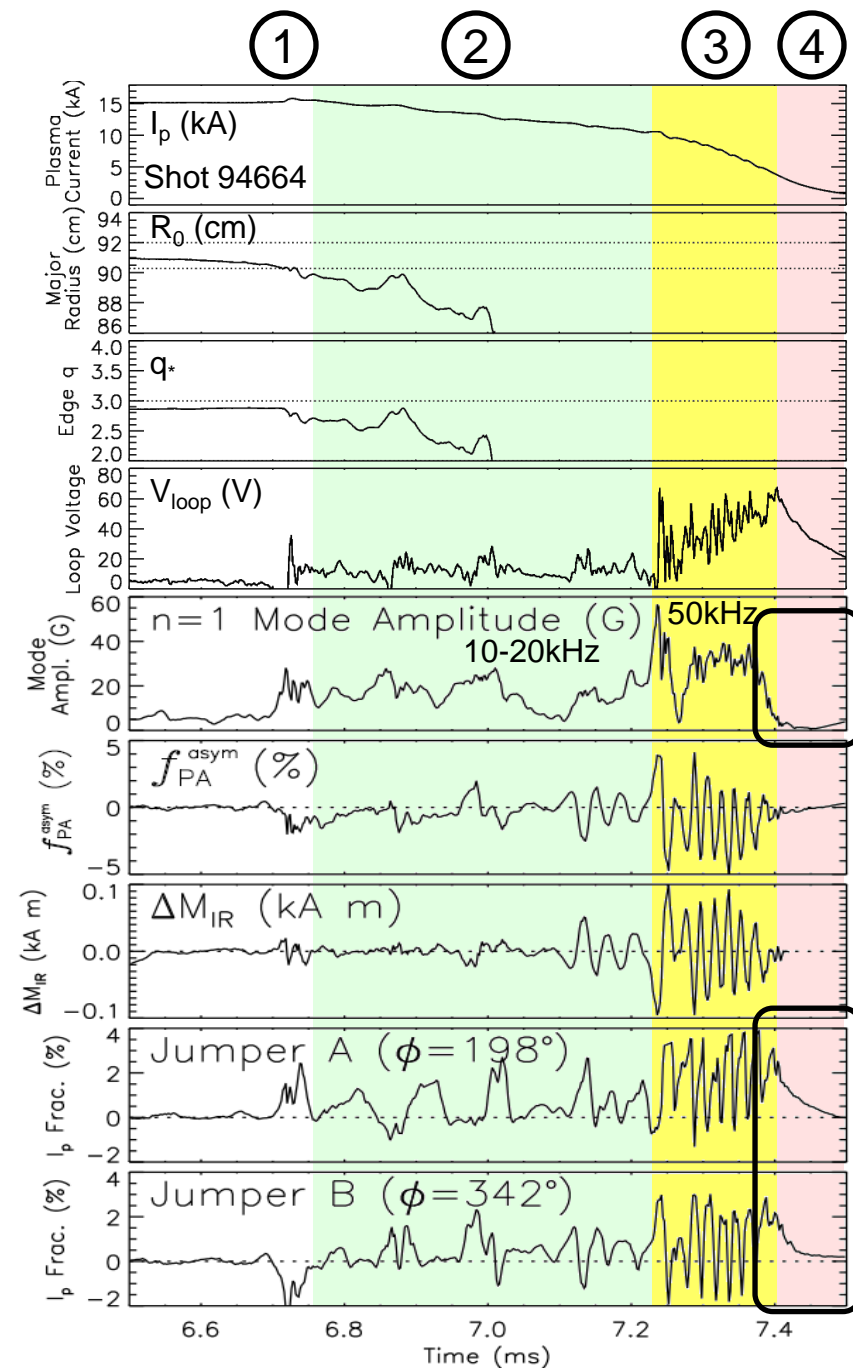
- Mode rotates at 10-20kHz
- Rotation is irregular

3. Fast I_p decay

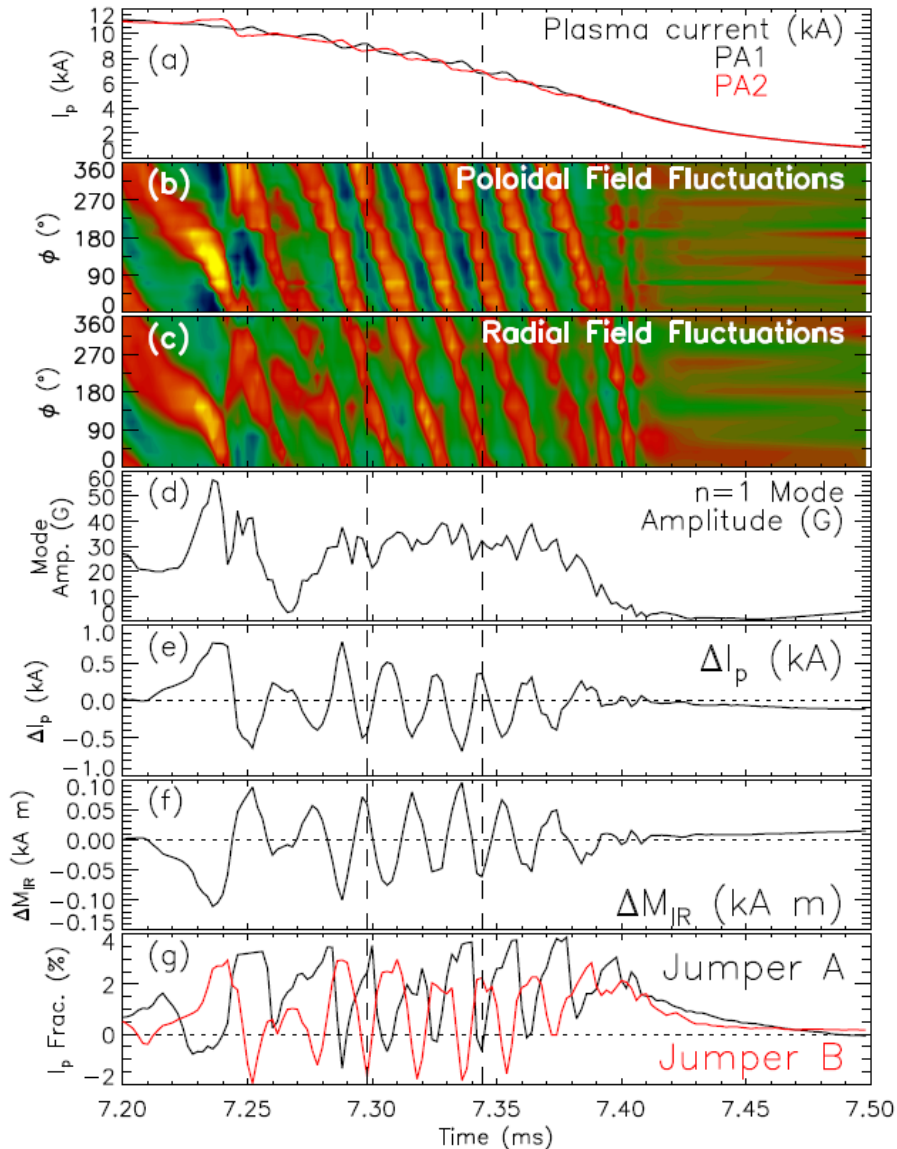
- Fast halo current rotation at ~50kHz
- Rotation is smooth

4. Symmetric vessel currents

- Co- I_p vessel currents conduct across insulating breaks after mode decays

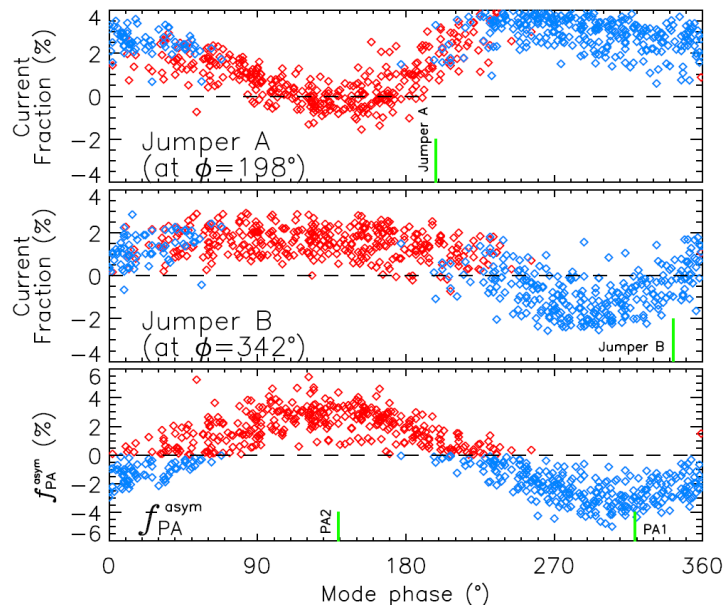
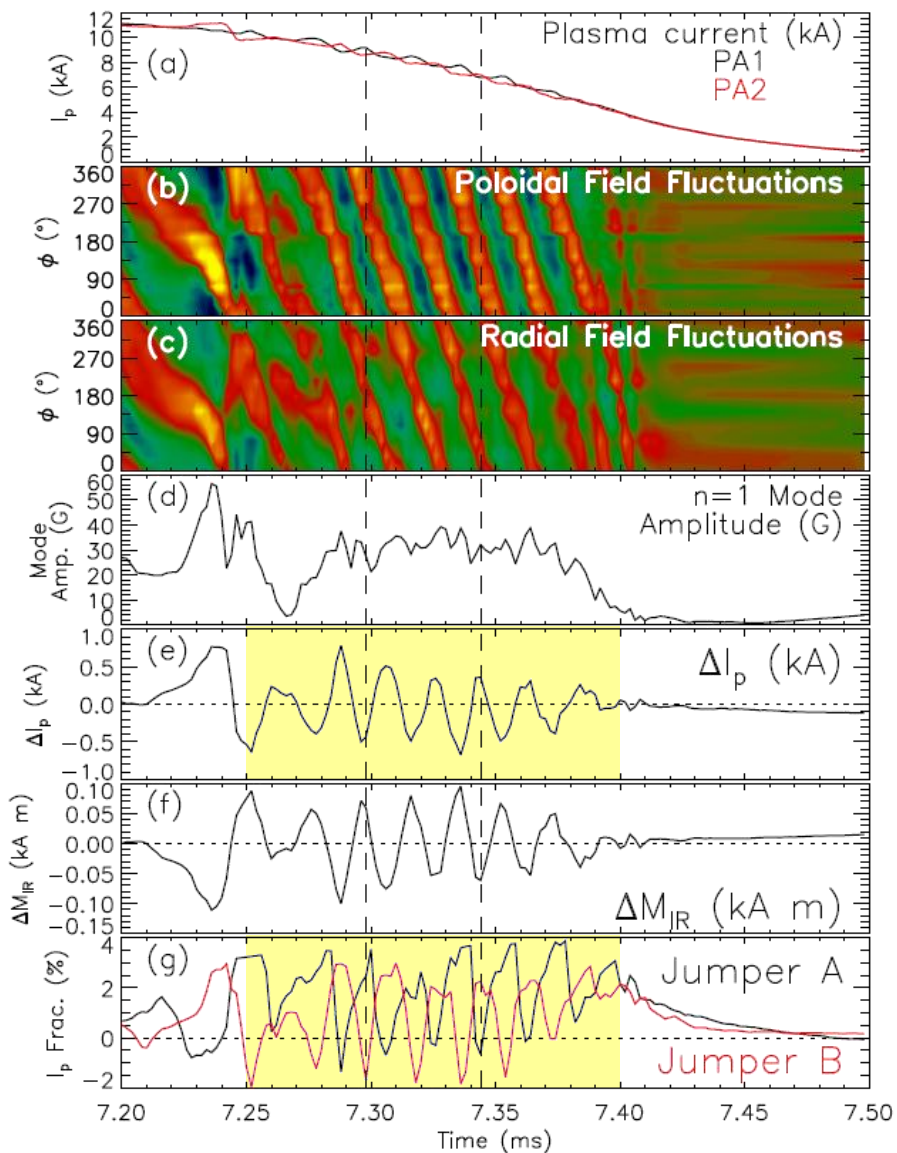


High frequency mode during fast CQ ramp accompanies the largest current asymmetries in HBT-EP

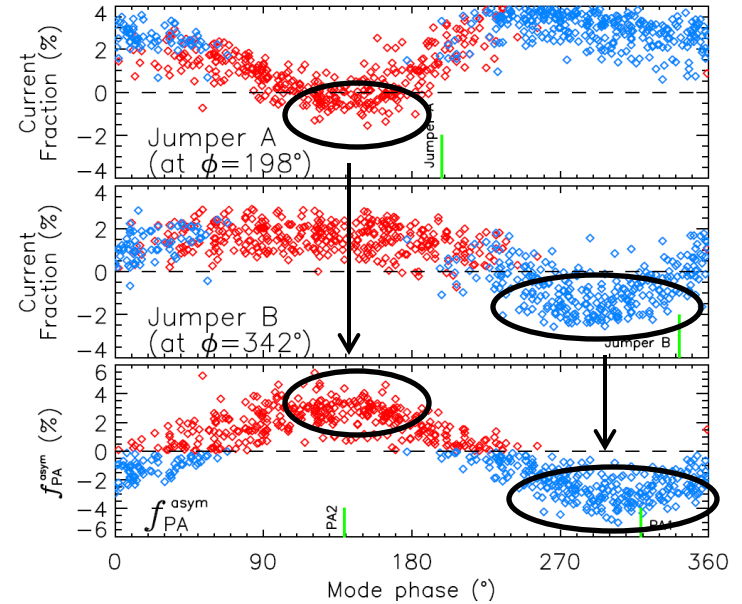
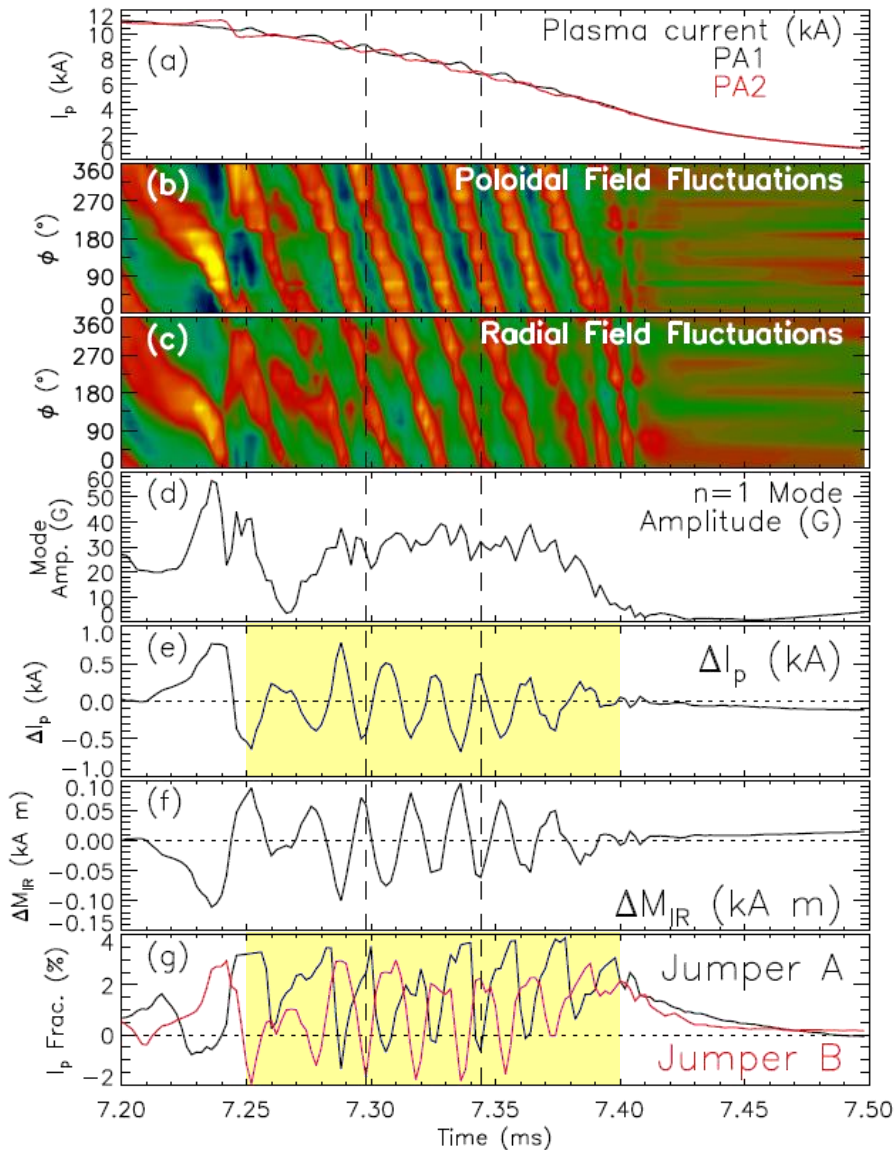


- Coherent mode rotating at $\sim 50\text{kHz}$

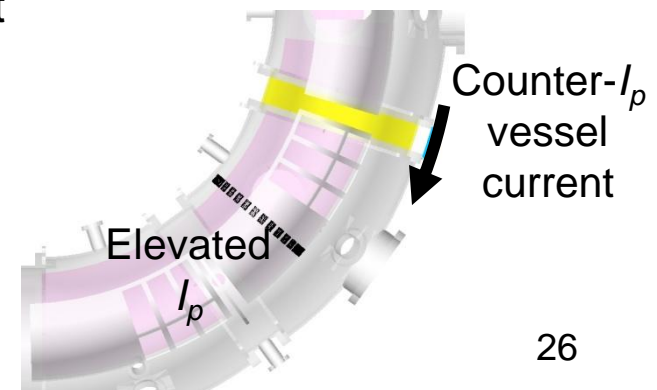
Clear phase relation exists between I_p asymmetry and toroidal vessel currents



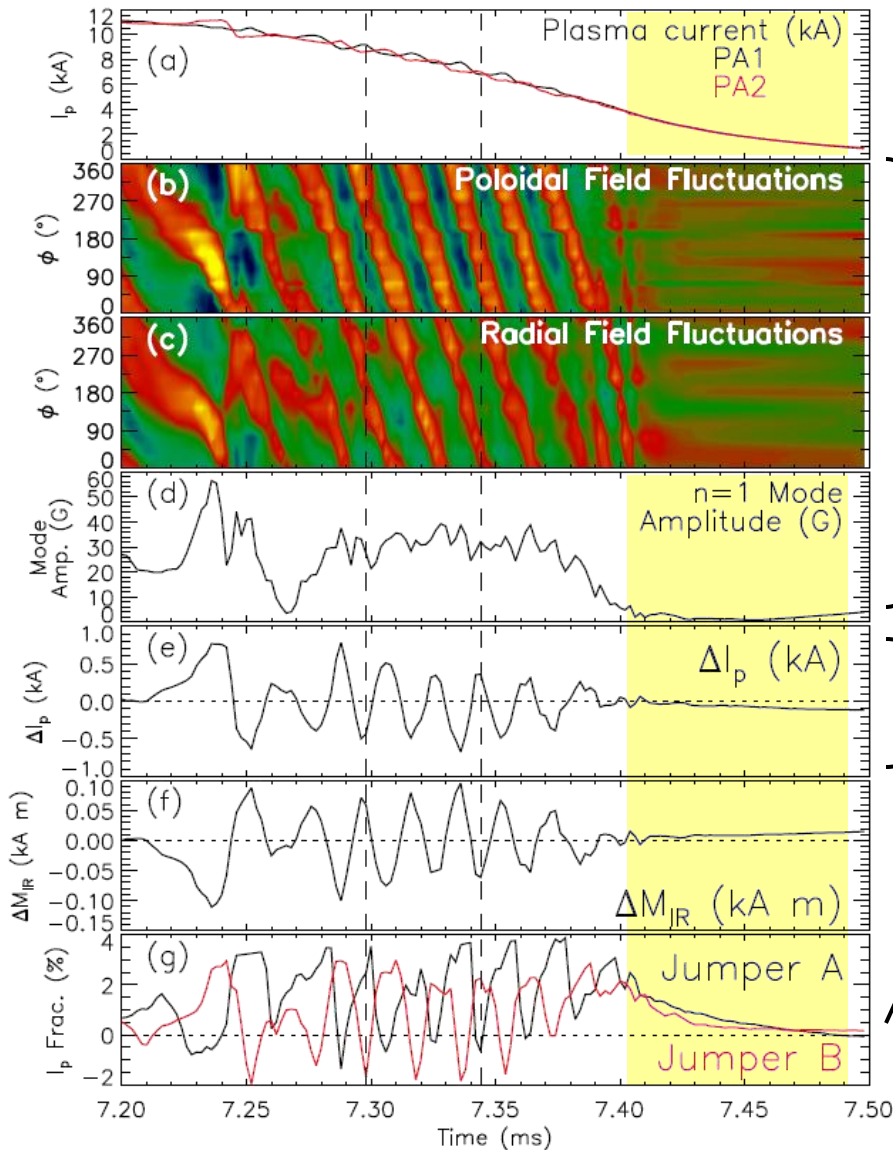
Clear phase relation exists between I_p asymmetry and toroidal vessel currents



- Local I_p is higher when nearest toroidal jumper has its most negative current



Jumper currents symmetrize in co- I_p direction at end of the current quench



- n=1 mode decays without evidence of locking

- I_p asymmetry vanishes

- Jumper currents remain significant

- Current must flow across SOL to bridge chamber sections

Outline



- HBT-EP device overview
 - Scrape-off layer current (SOLC) diagnostics and vessel geometry
 - Discharge characteristics
- Measurements during routine kink mode activity
- Measurements during disruptions
- Interpretation in context of WTKM and ATEC models
- Upcoming simulation and experiments

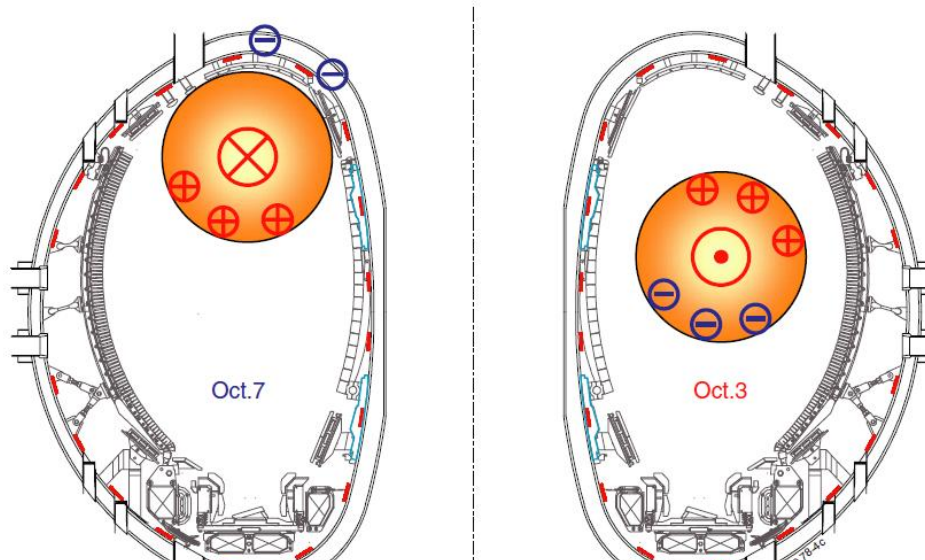
How do HBT-EP measurements compare to models of SOL/vessel currents during disruptions?



- WTKM and ATEC models are considered
- Models yield contrary predictions for the sign of strong toroidal vessel currents
 - WTKM predicts mostly counter- I_p currents
 - ATEC predicts mostly co- I_p currents
- Disclaimers:
 - This is my personal interpretation of each model
 - Not considering other models

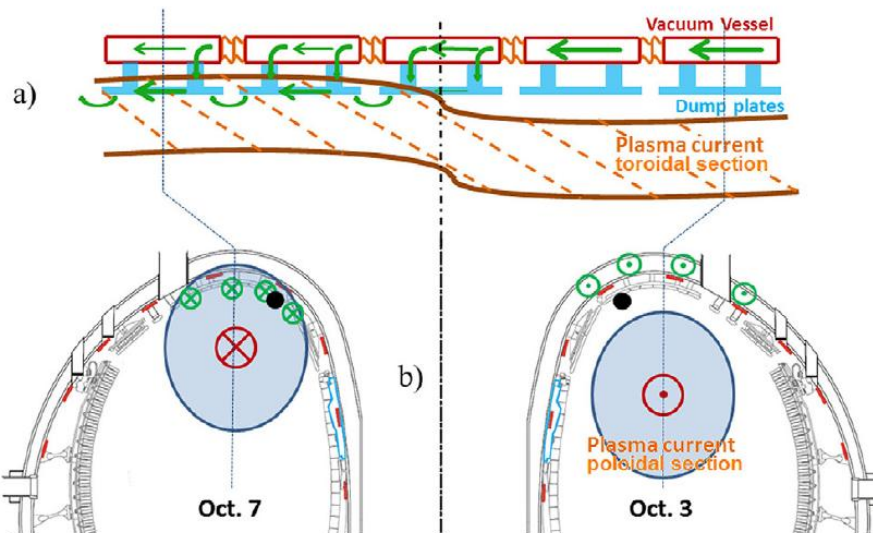
WTKM vs ATEC models for upward VDEs in JET

WTKM



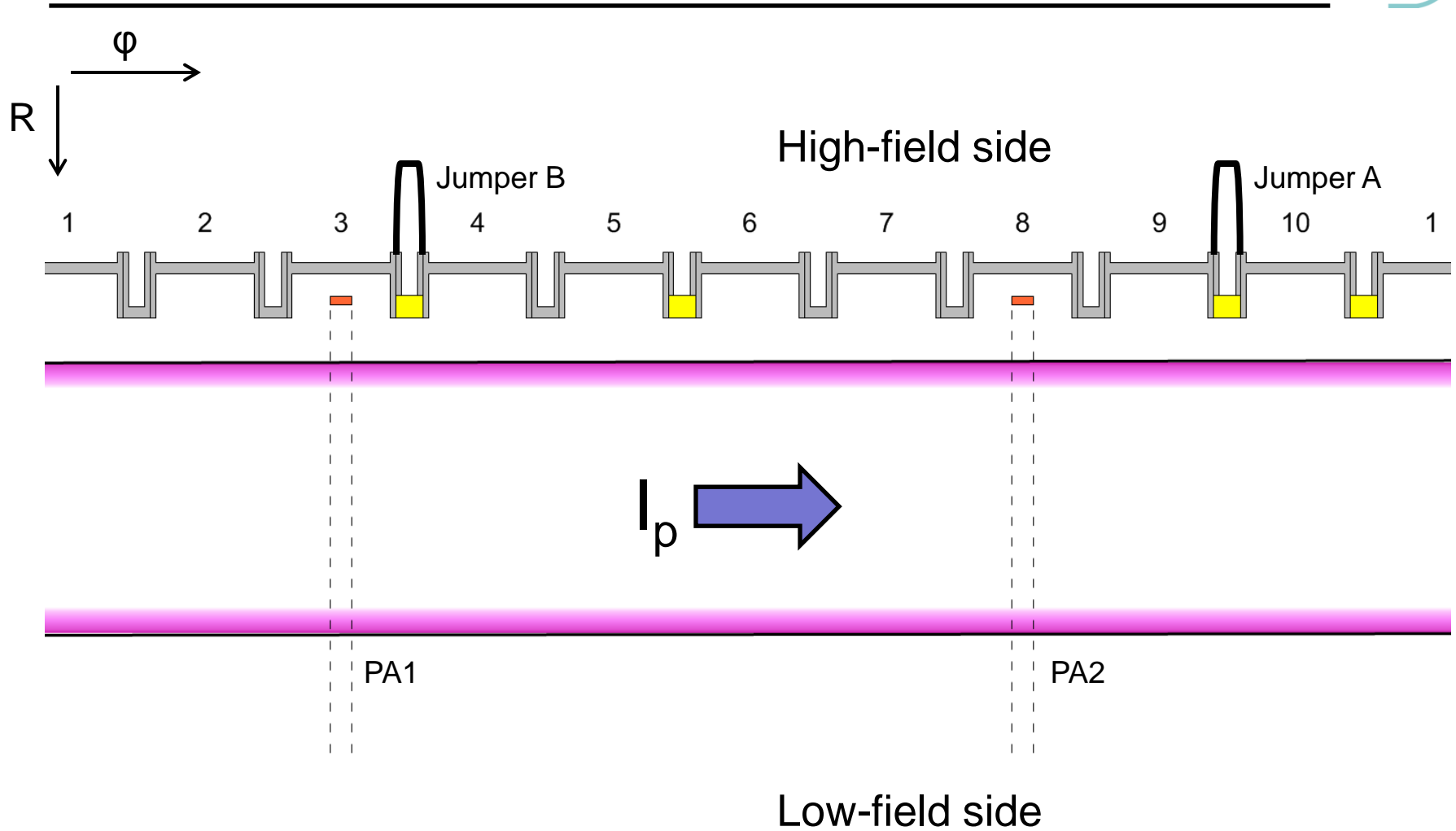
- Surface current generated in response to kink will conduct through the vessel upon contact

ATEC

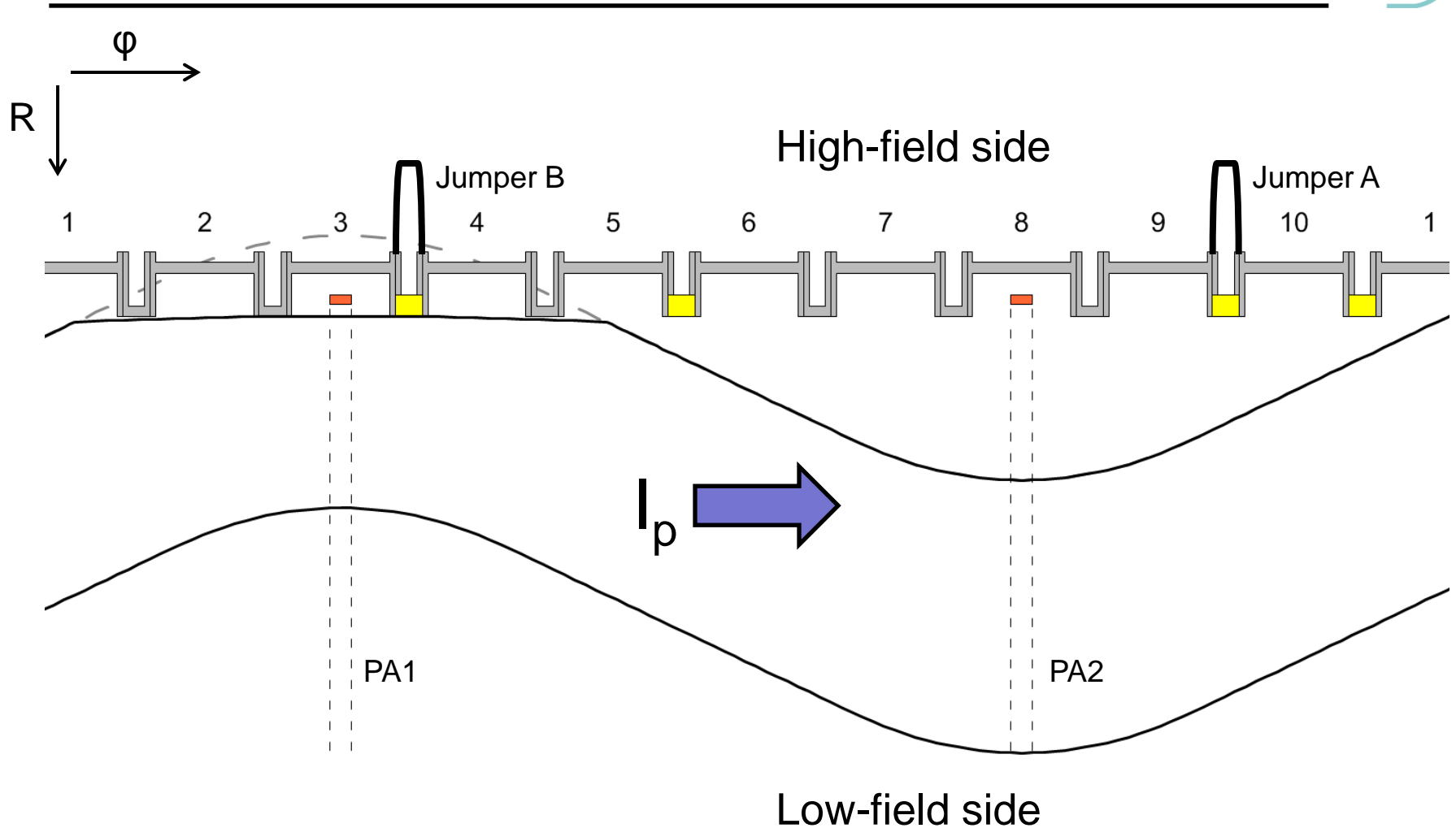


- Vessel eddy current from decaying I_p partially conducts through the plasma upon plasma-wall contact (shorting across tile gaps)

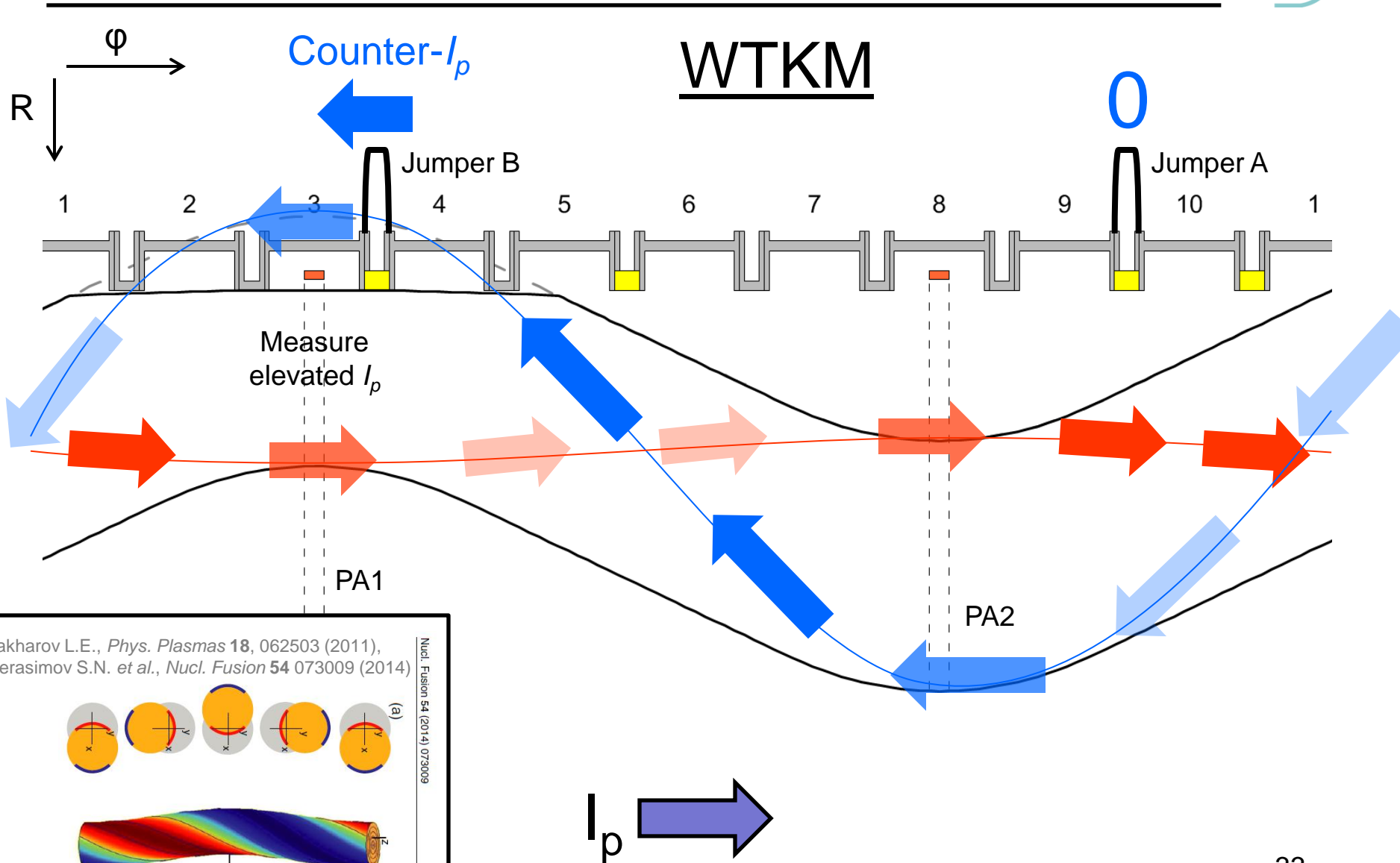
Expected currents in response to disruption kinks in HBT-EP



Expected currents in response to disruption kinks in HBT-EP



Expected currents in response to disruption kinks in HBT-EP

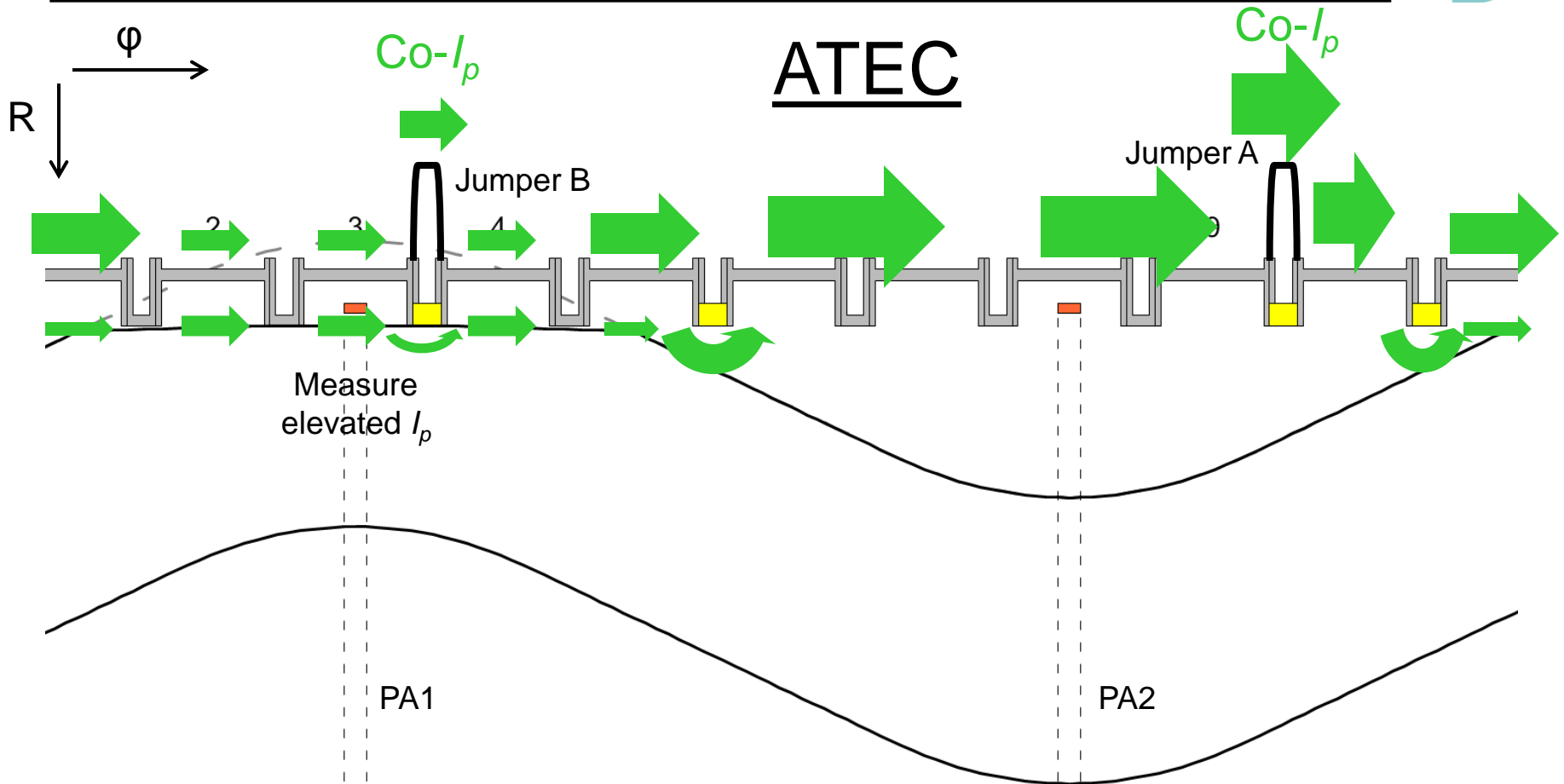


Zakharov L.E., *Phys. Plasmas* **18**, 062503 (2011),
 Gerasimov S.N. et al., *Nucl. Fusion* **54** 073009 (2014)

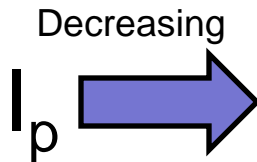
Nucl. Fusion **54** (2014) 073009

(a)

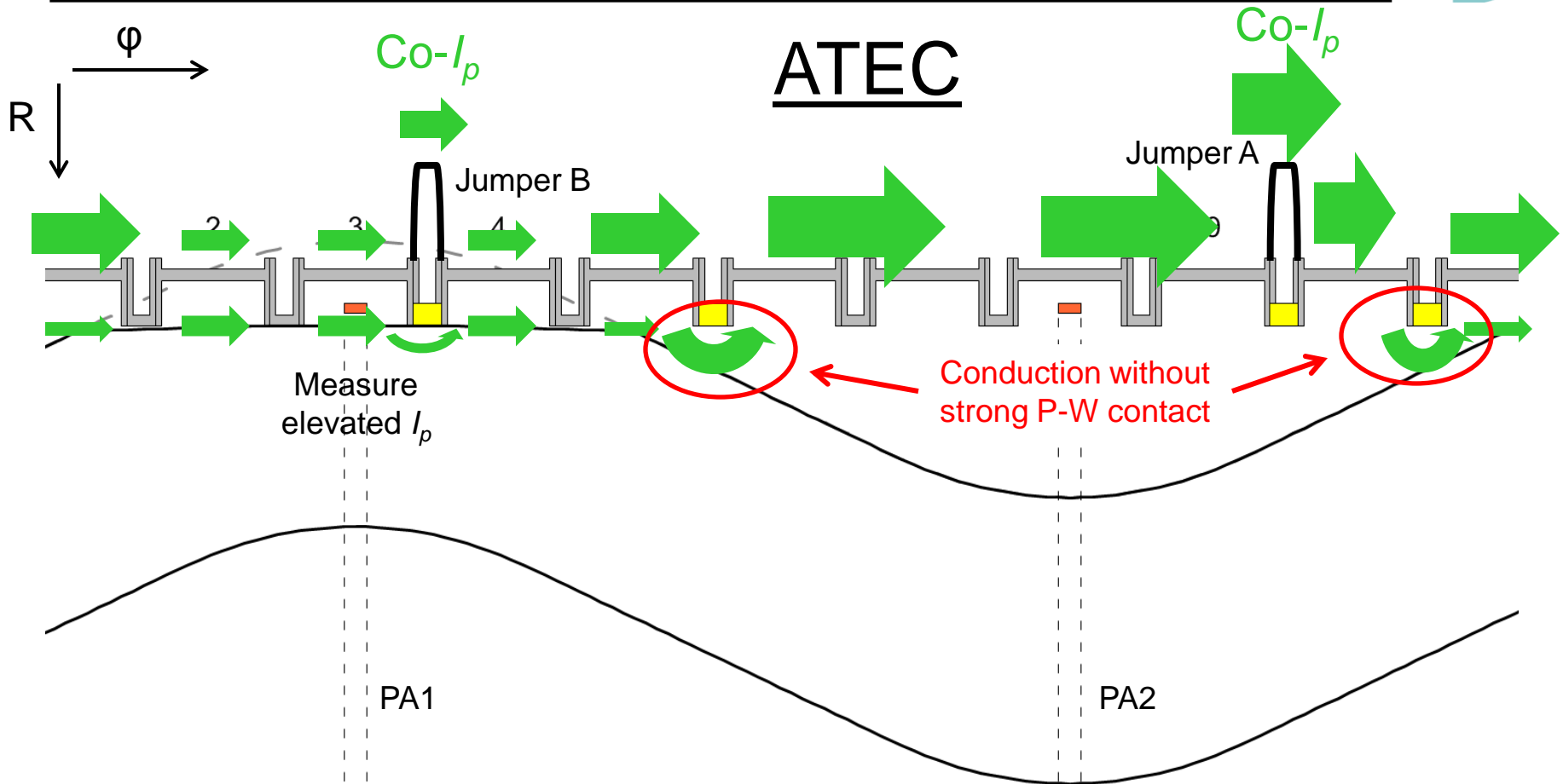
Expected currents in response to disruption kinks in HBT-EP



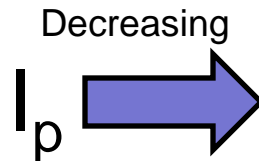
- Using ATEC as formulated for JET, with no plasma motion



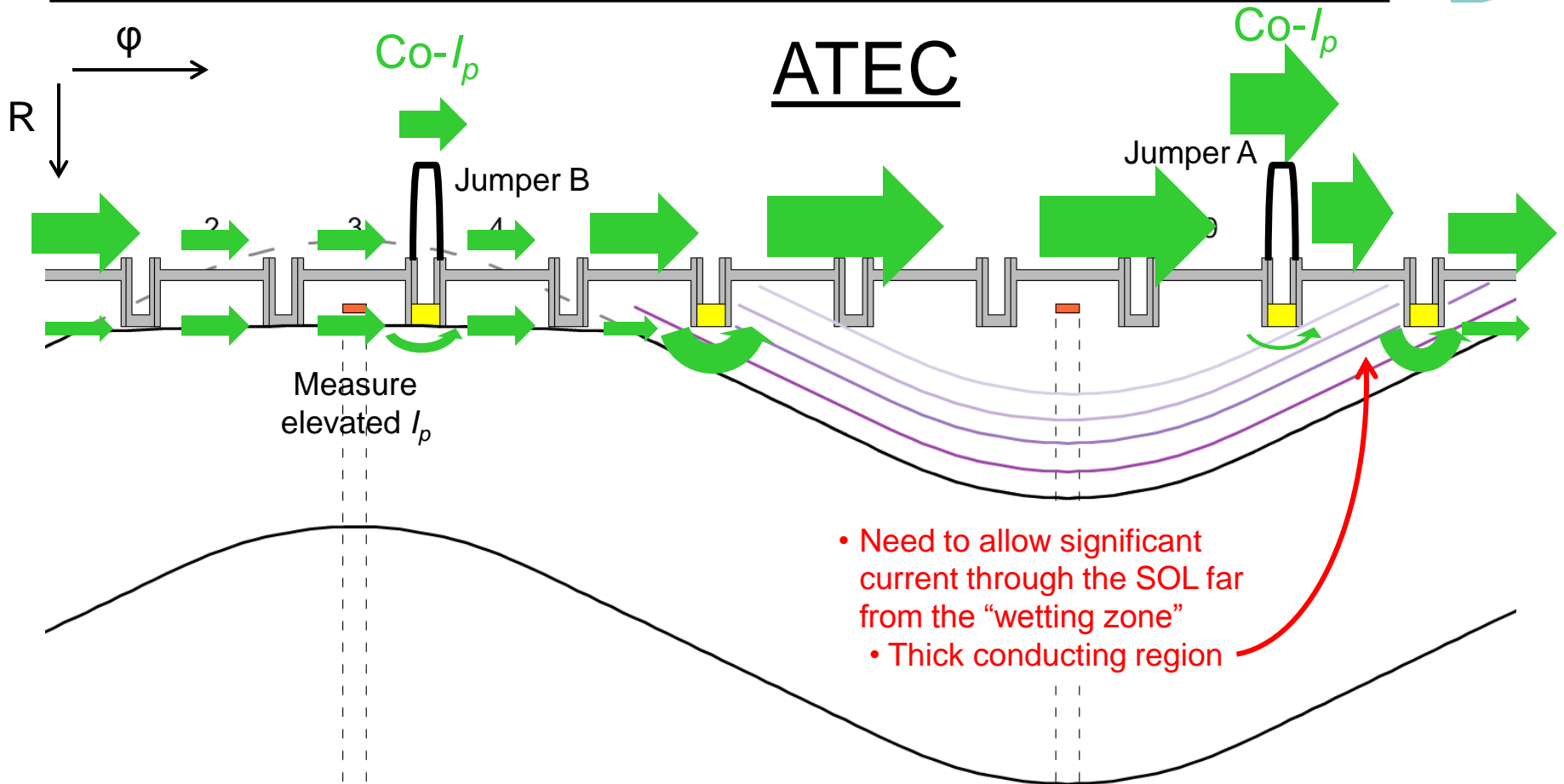
Expected currents in response to disruption kinks in HBT-EP



- Using ATEC as formulated for JET, with no plasma motion

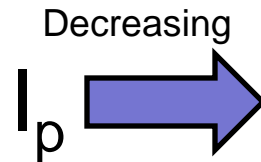


Expected currents in response to disruption kinks in HBT-EP



- Need to allow significant current through the SOL far from the “wetting zone”
- Thick conducting region

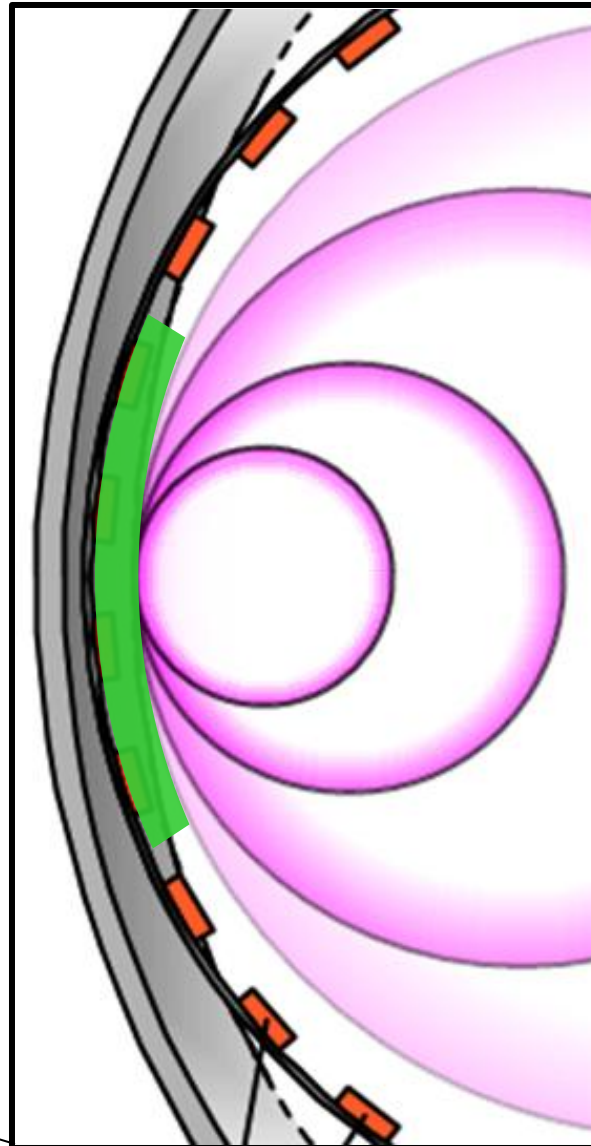
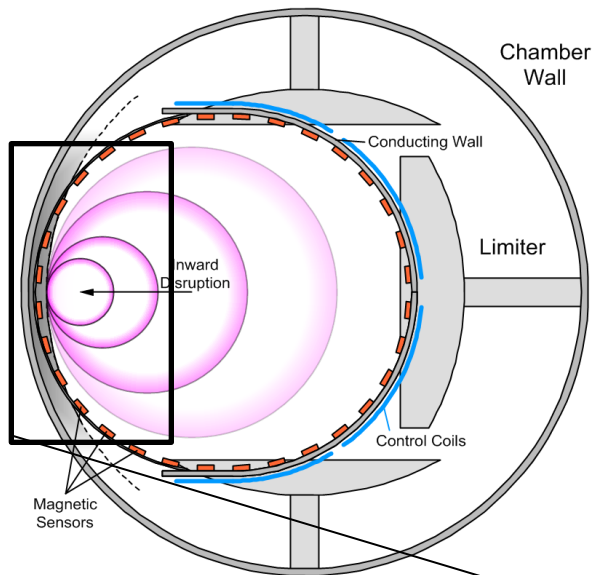
- Using ATEC as formulated for JET, with no plasma motion



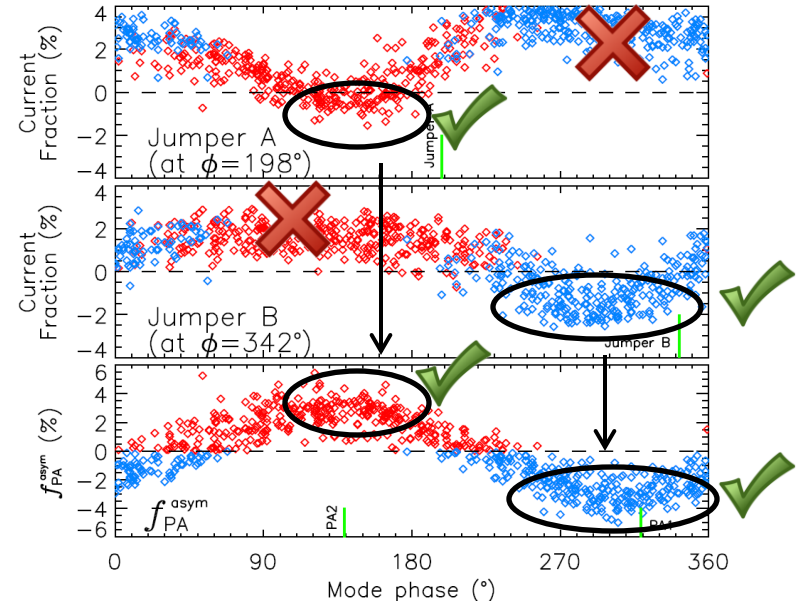
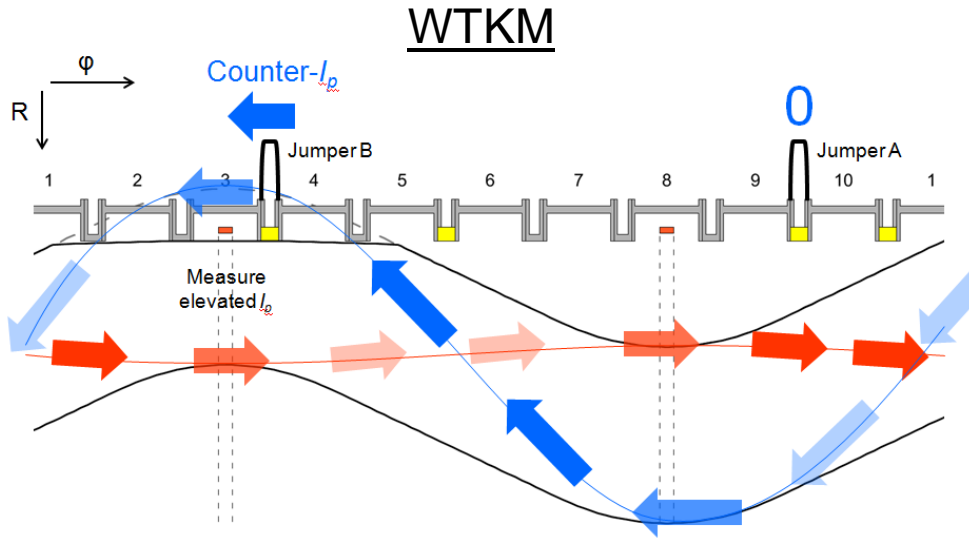
ATEC current responsible for elevated I_p measurement needs to flow in a ~1cm thick SOL region



- No bulk conducting materials exist between poloidal array sensors and LCFS
 - Only 64 μ m thick SS shimstock shielding in front of sensors

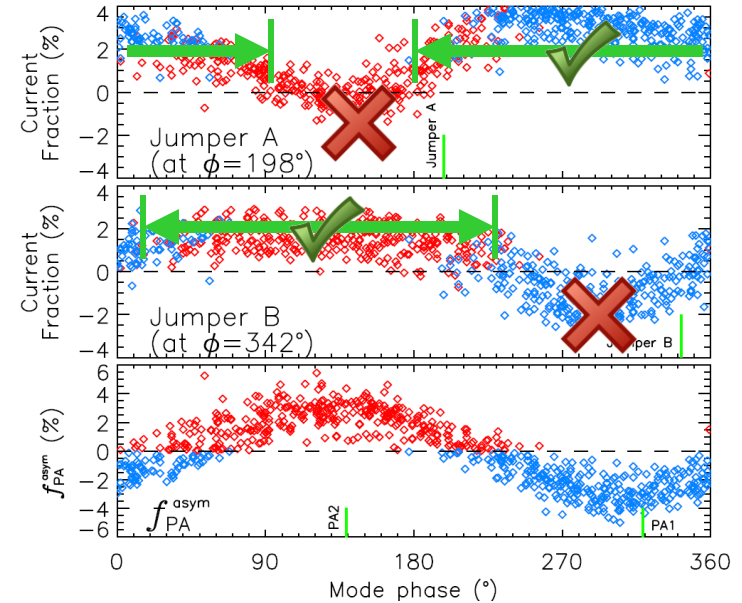
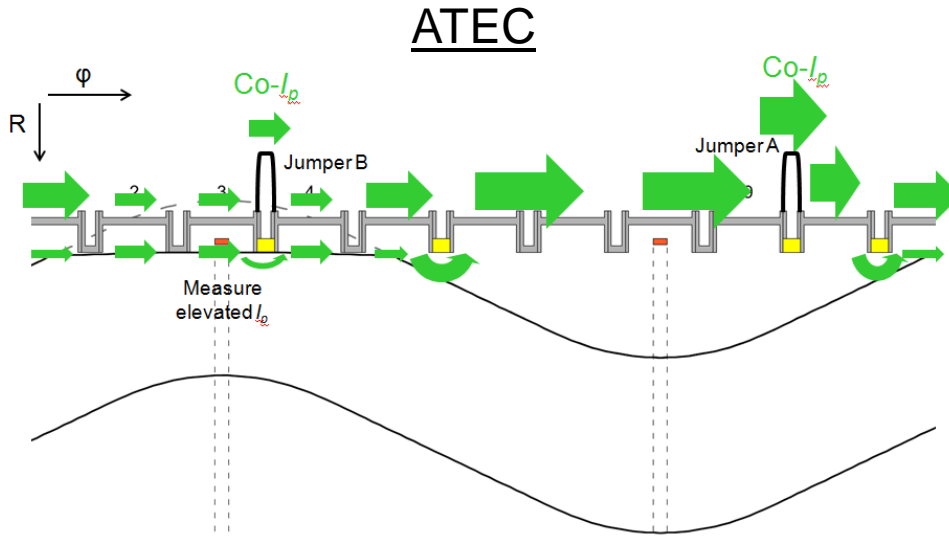


Evaluation of WTKM model



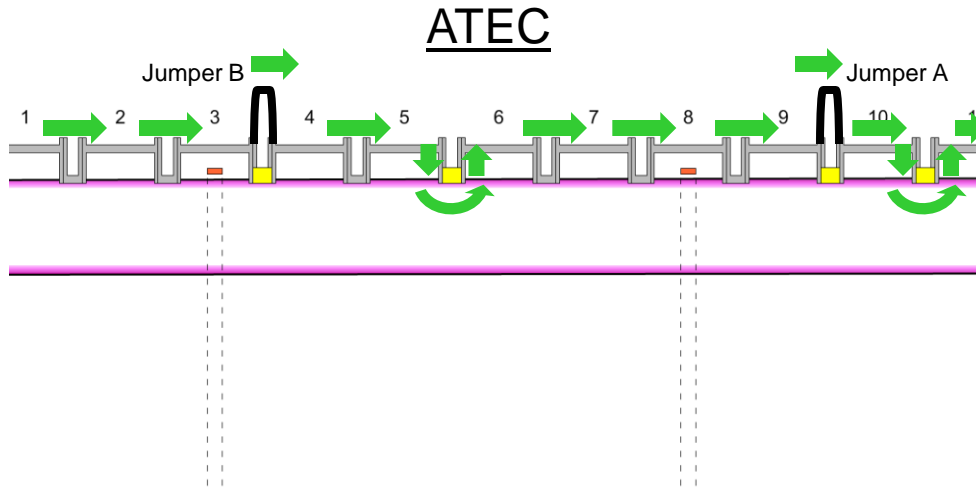
- Local Counter- I_p vessel current agrees with elevated I_p measurement
- Large Co- I_p vessel current is not predicted
 - Co- I_p “Evans” current is allowed, but should not be strong
 - Source-limited from plasma dissipation¹: $I^{\text{Ev}} \leq e \frac{dN_e}{dt}$
 - Co- I_p wall current should not extend to opposite side of vessel
 - Consider allowing very broad contact area and strong co- I_p halo current

Evaluation of ATEC model

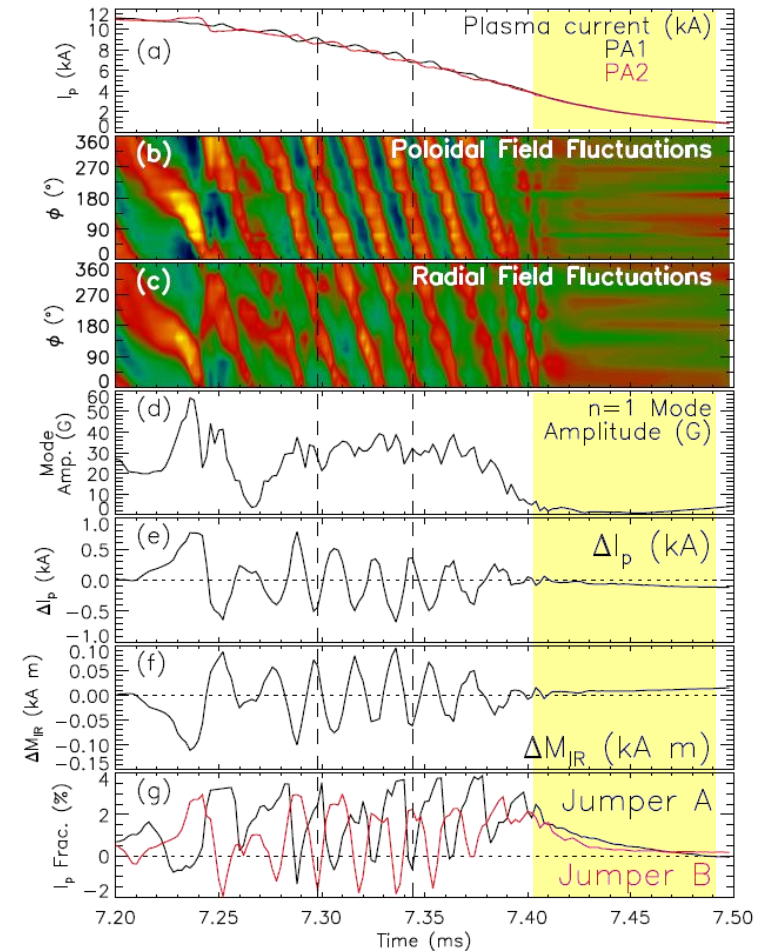


- Measured jumper currents are $co-I_p$ for most of the disruption duration
- ATEC Predicts $co-I_p$ jumper current where I_p is elevated
 - Current in local jumper would be lower than in the other jumper, but both still $co-I_p$
- Neglecting plasma motion, there should be no counter- I_p jumper current
 - Allowing counter- I_p currents induced by plasma motion could overpower $co-I_p$ current from I_p decay
- Strong $co-I_p$ current must flow in a relatively thin SOL region in front of poloidal array sensors

ATEC concept of toroidal eddy current flowing through SOL could explain symmetric current at end of CQ



- Current passing through jumpers must conduct to neighboring vessel sections through the SOL



Outline

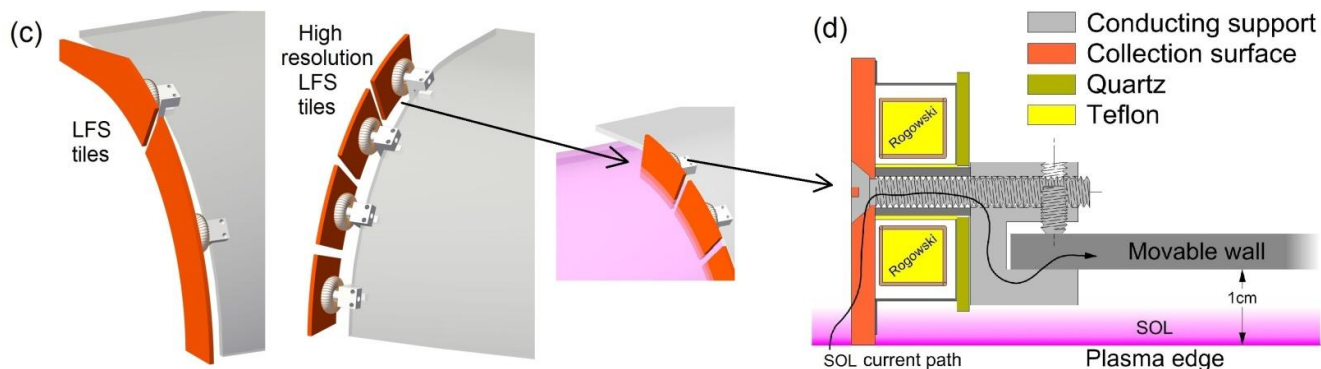
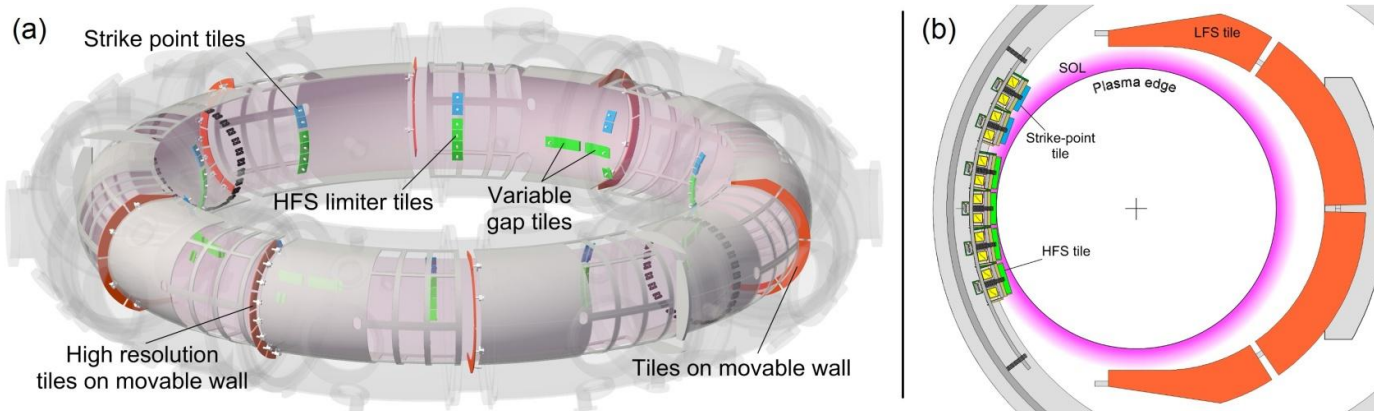


- HBT-EP device overview
 - Scrape-off layer current (SOLC) diagnostics and vessel geometry
 - Discharge characteristics
- Measurements during routine kink mode activity
- Measurements during disruptions
- Interpretation in context of WTKM and ATEC models
- Upcoming simulation and experiments

Upcoming simulation and experiments



- VALEN/IVB modeling
 - Compare direct source/sink currents versus vessel currents due to rotating kink mode eddy currents
- ATEC calculations for HBT-EP
- Upgraded SOLC diagnostics for further experiments:



Summary



- Direct measurements of toroidal vessel currents reveal asymmetric, oscillating *co-* and *counter-* I_p wall currents during kink modes and disruptions
 - Insulating breaks constrain vessel current to complete its circuit through SOL plasma
 - Currents reach $\sim 4\%$ of I_p during disruptions.
- I_p asymmetry characteristics agree with JET results¹ and ITER modeling²
 - Slope of asymmetry $\Delta I_p / \Delta M_{IR,IZ}$ scales like $1/a$
- WTKM³ and ATEC⁴ models can qualitatively explain some HBT-EP measurements, but each model has deficiencies as formulated.
 - *Both* ATEC and WTKM concepts are significant for vessel currents
 - Both models also have problems explaining some of the observations
 - Each model can qualitatively explain observed plasma current asymmetries
 - Conditions for ATEC appear more restrictive overall
- Upcoming experiments will improve validation of disruption current models

[1] Gerasimov S.N. *et al.*, *Nucl. Fusion* **54** 073009 (2014)
[2] Roccella R. *et al.*, “Modelling ITER asymmetric VDEs through asymmetries of toroidal eddy currents” IAEA FEC [EX/P6-40] (2016)

[3] Zakharov L.E. *et al.*, *Phys. Plasmas* **19** 055703 (2012)
[4] Roccella R. *et al.*, *Nucl. Fusion* **56** 106010 (2016)

* Levesque, J.P. *et al.*, *Nucl. Fusion* **57** 086035 (2017)